

GROUP TUTORING SESSIONS

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1 Problem Set on Numerical Methods

1.1 Using Mathematica[®] in Optics: an introduction

The following is a list of resources available to help you navigate the software:

- **Mathematica basics**, by James Stewart from *CalcLabs with Mathematica: single variable calculus*. This book chapter describes many of the most important and basic elements of Mathematica[®] and discuss a few of the more common technical issues related to using Mathematica[®].
This Mathematica[®] text is suggested for first-time users.
- **Mathematica tutorial**, by Mark S. Gockenbach. To accompany *Partial differential equations: analytical and numerical methods* [1].
This tutorial is my suggested text for students who have minor experience using Mathematica[®].
- **Comprehensive documentation** for Mathematica[®] and the Wolfram Language, which includes details and examples for functions, symbols, and workflows.
- **Wolfram demonstrations project**. Explore thousands of free applications across science, mathematics, engineering, technology, and more.
- **Wolfram library archive** has thousands of downloadable resources for Mathematica, collected over the full history of Wolfram.

This is a list of resources available in Spanish:

- **Guía rápida para el nuevo usuario de Mathematica 5.0[®]**, by Eugenio M. Fedriani Martel and Alfredo García Hernández-Díaz.
- **Breve manual de Mathematica 5.1**, by Robert Ipanaqué Chero and Ricardo Velesmoro León.
- **Docencia con Mathematica**, by Javier Pérez (Departamento de Análisis Matemático, Universidad de Granada).

1.1.1 Plotting scalar and vector wave fields

Consider the electric field of a time-harmonic plane wave propagating along the z axis in a vacuum. The electric field $\mathbf{E}(z, t) = \text{Re}[\vec{E}(z, t)]$ can be determined by means of its analytical representation $\vec{E}(z, t) = \hat{\sigma}E(z, t)$, where $E(z, t) = E_0 \exp(ik_0z - i\omega t)$. Here, $k_0 = \omega/c$ is the vacuum wavenumber, and the unit vector $\hat{\sigma} = \sigma_x \hat{x} + \sigma_y \hat{y}$ gives the state of polarization (here, $\hat{\sigma}$ is equivalent to the Jones vector), where $|\sigma_x|^2 + |\sigma_y|^2 = 1$. For numerical purposes, set the amplitude $E_0 = 1$ V/m and the vacuum wavelength $\lambda_0 = 500$ nm (where $k_0 = 2\pi/\lambda_0$), and $c = 3 \cdot 10^8$ m/s.

First, consider a linearly-polarized plane wave, $\hat{\sigma} = \hat{\sigma}^*$. In practical terms, the electric field can be represented by the scalar wave function $E(z, t)$.

1. Plot $\text{Re}[E(z, t)]$ and $|E(z, t)|^2$ within the range $0 \leq z \leq 2\lambda_0$ at the instants $t = 0$ and $t = T/4$, where T is the period of the oscillation, that is, $\omega = 2\pi/T$.
Hint: use the built-in symbol `Plot[]`.
2. Plot $\text{Re}[E(z, t)]$ within the range $0 \leq z \leq 2\lambda_0$ and $0 \leq t \leq 2T$.
Hint: use the built-in symbols `Plot3D[]` and `ContourPlot[]`.

Next, consider a circularly-polarized plane wave with $\hat{\sigma} = (\hat{x} + i\hat{y})/\sqrt{2}$.

3. Show the locus traced by the tip of the electric field $\text{Re}[\vec{E}(z, t)]$ at a given point of the plane $z = 0$ through one cycle, for instance within $0 \leq t \leq T$, by using a two-dimensional (2-D) plot, which generates the so-called *ellipse of polarization*.
Hint: use the built-in symbol `ParametricPlot[]`.
4. Show again the locus traced by the tip of $\text{Re}[\vec{E}(z, t)]$ at $z = 0$ within the interval $0 \leq t \leq 3T$, however using a 3-D plot, for the same circularly-polarized plane wave. Can you infer from this figure the polarization handedness of the light: right circular or left circular? Also, create a 3-D graph of the locus traced by the tip of $\text{Re}[\vec{E}(z, t)]$, now set at the instance $t = 0$ and evaluated along the z axis, within the interval $0 \leq z \leq 3\lambda_0$.
Hint: use the built-in symbol `ParametricPlot3D[]`.
5. Plot the time evolution of the vector field $\text{Re}[\vec{E}(z, t)]$ at different points of the plane $z = 0$ (for instance, in the domain $|x|, |y| \leq 1$ mm) for the same circularly-polarized plane wave.
Hint: use the built-in symbol `VectorPlot[]` to generate a vector plot of the vector field $\text{Re}[\vec{E}]$ as a function of x and y , and the built-in symbol `Animate[]` to generate an animation where t varies continuously from 0 to T .

1.1.2 Solving second-order linear homogeneous ODEs

Consider a half-space $z < 0$ filled with an isotropic, homogeneous, lossless, dielectric material of index of refraction n_1 . Also, in the half-space $z > 0$ the medium is isotropic and homogeneous with index of refraction n_2 , which is not necessarily real valued but $\text{Re}[n_2] \geq 0$ is assumed without loss of generality. Finally, the photonic system is free of charges and currents.

In the semi-space $z < 0$, a 1-D time-harmonic electric field $\vec{E}(z) \exp(-i\omega t)$ satisfies the following second-order linear homogeneous ordinary differential equation (ODE) with constant coefficients,

$$\left[\frac{\partial^2}{\partial z^2} + k_1^2 \right] \vec{E}(z) = 0, \quad (1.1.1)$$

which is the so-called *Helmholtz equation*, where $k_1 = n_1 k_0$ ($k_0 = \omega/c$) is the wavenumber in the medium. Furthermore, one may show that $\vec{E}(z) = \hat{\sigma} E(z)$, where

$$E(z) = E_0 [\exp(ik_1 z) + r \exp(-ik_1 z)], \quad (1.1.2)$$

is a solution of the 1-D Helmholtz equation in $z < 0$, where $\hat{\sigma}$ is a complex, unitary ($\hat{\sigma} \cdot \hat{\sigma}^* = 1$), transverse ($\hat{\sigma} \cdot \hat{z} = 0$) vector denoting the state of polarization of the wave field, and E_0 and r are complex-valued constants. The electric field given in Eqs. (1.1.2) represents a superposition of two counter-propagating plane waves: the *incident* wave has an electric field with amplitude E_0 , and thus intensity $n_1 S_0 = \frac{1}{2} n_1 |E_0|^2 / Z_0$ ($Z_0 = \sqrt{\mu_0 / \epsilon_0}$ is the intrinsic impedance of a vacuum), which propagates along the z axis in direction to the interface set at $z = 0$, whereas the *reflected* wave propagates back from the interface having an amplitude $r E_0$. In fact, r is the well-known reflection coefficient, which can be estimated by means of

$$r = \frac{E(0)}{E_0} - 1, \quad (1.1.3)$$

and $R = |r|^2$ gives the wave reflectance. Furthermore, the complex Poynting vector, $\vec{S}(z) = \frac{1}{2} \vec{E}(z) \times \vec{H}^*(z) = \hat{z} S_z(z)$, has its real part, as measured at $z = 0$, given by $\text{Re}[S_z(0)] = n_1 S_0 (1 - |r|^2)$.

In the half-space $z > 0$, the 1-D electric field satisfies the Helmholtz equation, $(\partial_z^2 + k_2^2) \vec{E}(z) = 0$, where $k_2 = n_2 k_0$ is the wave number in this medium. One may verify the validity of the solution $\vec{E}(z) = \hat{\sigma} E(z)$ to the Helmholtz equation, where

$$E(z) = E_0 t \exp(ik_2 z), \quad z > 0. \quad (1.1.4)$$

and the unit vector $\hat{\sigma}$ represents the same state of polarization of the incident and reflected fields. The electric field given in Eq. (1.1.4) represents a plane wave propagating along the z axis away from the interface set at $z = 0$. In addition, t is the complex-valued transmission coefficient, which can be estimated by $t = E(0)/E_0 = 1 + r$. Finally, the complex Poynting vector has its real part, as evaluated at the boundary $z = 0$, which is given by $\text{Re}[\vec{S}(0)] = \hat{z} S_0 |t|^2 \text{Re}(n_2)$. Therefore, $T = |t|^2 \text{Re}(n_2)/n_1$ gives the wave transmittance. Note that $T + R = 1$ by conservation of energy.

1. Show that the electric field in the half-space $z < 0$ satisfies the Robin-type boundary condition

$$\left[ik_1 E(z) + \frac{\partial E(z)}{\partial z} \right]_{z=z_1} = 2ik_1 E_0 \exp(ik_1 z_1), \quad (1.1.5)$$

which is established at any transverse plane $z = z_1$, called *input port*, provided that $z_1 < 0$. In the half-space $z > 0$, the electric field satisfies the *Sommerfeld radiation condition*,

$$\left[ik_2 E(z) - \frac{\partial E(z)}{\partial z} \right]_{z=z_2} = 0, \quad \text{and} \quad z_2 > 0, \quad (1.1.6)$$

which is established at the *output port*, $z = z_2$.

For numerical purposes, set the amplitude $E_0 = 1$ V/m, the vacuum wavelength $\lambda_0 = 500$ nm (where $k_0 = 2\pi/\lambda_0$), and $c = 3 \cdot 10^8$ m/s. Also set the input and output ports at $z_2 = -z_1 = 2\lambda_0$.

2. Find numerically the solution to the second-order linear homogeneous ODE,

$$\left[\frac{\partial^2}{\partial z^2} + k_0^2 n^2(z) \right] E(z) = 0, \quad \text{where} \quad z_1 \leq z \leq z_2, \quad (1.1.7)$$

providing the z dependence of the electric field, $E(z)$, where $n(z) = n_1$ within $z_1 \leq z < 0$, and $n(z) = n_2$ within $0 < z \leq z_2$. Firstly use $n_1 = 1$ and $n_2 = 1.5$. Apply the Robin boundary condition (1.1.5) at the input port, and the radiation condition (1.1.6) at the output port.

Hint: use the normalized coordinate $x = k_0 z$, and the functions $u(x) = E(z)$ and $a(x) = n^2(z)$, to transform Eq. (1.1.7) into $\partial_x^2 u(x) + a(x)u(x) = 0$, to be used with the built-in symbol `NDSolve[]`.

Alternatively, one may take the following steps:

- use the normalized coordinate $x = k_0 z$, and the functions $u(x) = E(z)$, $a(x) = n^2(z)$, and $c = -1$, in order to transform Eq. (1.1.7) into the *coefficient form* $\nabla \cdot (-c \nabla u) + au = 0$ of ODEs, as managed by Mathematica®[®], to be used with the built-in symbol `NDSolve[]`.
- use the functions $q(x) = in(z)$ and $g(x) = 0$, both evaluated at the boundary $x_2 = k_0 z_2$, in order to transform Eq. (1.1.6) into the Robin boundary condition $\hat{n} \cdot (c \nabla u) = g - qu$ as treated by Mathematica®[®], and implement it by means of the built-in symbol `NeumannValue[]`.

- use the functions $q(x) = in(z)$ and $g(x) = 2in(x)E_0 \exp[in(x)x]$, both evaluated at the boundary $x_1 = k_0 z_1$, in order to transform Eq. (1.1.5) into the Robin boundary condition $\hat{n} \cdot (c\nabla u) = g - qu$ as treated by Mathematica[®], to be implemented by `NeumannValue[]`.
3. Plot the real and imaginary part of the wave function $E(z)$ (or $u(x)$) which was found previously. Also plot $|E(z)|$ within the region of computation.
Hint: use the built-in symbol `ReImPlot[]`.
 4. Find numerically the reflection coefficient r given in Eq. (1.1.3), and compare with the analytical expression

$$r = \frac{n_1 - n_2}{n_1 + n_2}. \quad (1.1.8)$$

Estimate the reflectance and transmittance by using your numerical results, and also compare it with the theoretical predictions.

5. Repeat 2–4 assuming now that $n_2 = 0.055 + i4.0$ (silver at $\lambda_0 = 600$ nm). For a better convergence of the numerical evaluation, set $z_2 = \lambda_0/2$ to shift the output port closer to the vacuum/silver interface, and use the Dirichlet boundary condition $E(z) = 0$ at $z = z_2$.
Hint: use the built-in symbol `DirichletCondition[]`.

1.1.3 The Fourier transform, the Fourier series expansion and the DFT

Let us consider an optical signal characterized by a 1-D function $f(t)$, where t may stand for the time coordinate. The Fourier transform (FT) of f can be represented by the symbol $\mathcal{F}(f)$ giving

$$\mathcal{F}(f)(\omega) = F(\omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{+\infty} f(t) \exp(i\omega t) dt, \quad (1.1.9)$$

where ω is the spectral coordinate in the Fourier domain. Some useful properties of the FT are:

- If $f_a(t) = f(t/a)$ then $\mathcal{F}(f_a)(\omega) = |a|F(a\omega)$.
- If $f_0(t) = f(t - t_0)$ then $\mathcal{F}(f_0)(\omega) = F(\omega) \exp(i\omega t_0)$.
- If $f_e(t) = f(t) \exp(-i\omega_0 t)$ then $\mathcal{F}(f_e)(\omega) = F(\omega - \omega_0)$.
- If $f'(t) = df(t)/dt$ then $\mathcal{F}(f')(\omega) = -i\omega F(\omega)$.
- $\mathcal{F}(f \otimes g)(\omega) = \sqrt{2\pi} F(\omega) G(\omega)$, where $(f \otimes g)(t) = \int_{-\infty}^{+\infty} f(t') g(t - t') dt'$.
- $\mathcal{F}(\mathcal{F}(f))(t) = f(-t)$. As a consequence, $f(t) = \mathcal{F}(F)(-t) = \mathcal{F}^{-1}(F)(t)$, where \mathcal{F}^{-1} is the inverse Fourier transform.
- *Plancherel theorem* (also called Parseval-Plancherel identity): $\int_{-\infty}^{+\infty} |f(t)|^2 dt = \int_{-\infty}^{+\infty} |F(\omega)|^2 d\omega$.

1. Find the FT of the following functions:

- * The rectangle function $f(t) = \text{rect}(t) = 1$ if $|t| < 1/2$, otherwise vanishing.
- * The sinc (or *sinus cardinalis*) function $F(\omega) = \text{sinc}(\omega) \equiv \sin(\omega)/\omega$.
- * The modulated time-harmonic signal $f(t) = \exp(-i\omega_0 t) \exp[-(t/\tau)^2]$, where $\tau > 0$ is the pulse length and $\omega_0 > 0$ is the so-called carrier frequency.
- * The time-limited Gaussian function $f(t) = \exp[-(t/\tau)^2] \text{rect}(t/\Delta t)$, where $\tau, \Delta t > 0$.

- * The normalized hyperbolic secant function $f(t) = \text{sech}(\sqrt{\pi/2}t)$.
- * The Dirac delta function $f(t) = \delta(t - t_0)$.
- * The Dirac comb function $f(t) = \text{comb}(t) = \sum_{n=-\infty}^{\infty} \delta(t - n)$.
- * The periodic function $f(t) = \cos^2(t)$.

Hint: use the built-in symbol `FourierTransform[]` (also `Integrate[]`). In addition, the option `Assumptions -> $\tau > 0$` can be applied to the modulated time-harmonic signal, to mention an example.

2. Plot $f(t)$ and $F(\omega)$ for the functions previously analyzed in 1. Allocate numerical values to the parameters τ , Δt , and ω_0 freely. In cases involving Dirac delta functions, one may use that $\delta(x) \rightarrow \varepsilon/[\pi(x^2 + \varepsilon^2)]$ in the limit $\varepsilon \rightarrow 0^+$.

Hint: use the built-in symbol `ReImPlot[]` for complex-valued functions.

In particular, a periodic function, $f_p(t + \Delta t) = f_p(t)$, has a Fourier series expansion given by

$$f_p(t) = \sum_{s=-\infty}^{+\infty} c_s \exp(-is\Delta\omega t), \quad \text{where} \quad c_s = \frac{1}{\Delta t} \int_{-\Delta t/2}^{\Delta t/2} f_p(t) \exp(is\Delta\omega t) dt, \quad (1.1.10)$$

is the Fourier coefficient of the s -th harmonic, and $\Delta\omega = 2\pi/\Delta t$ is the fundamental frequency. Therefore, its FT $F_p(\omega) = \mathcal{F}(f_p)(\omega)$ is characterized by a discrete but generally infinite number of coefficients c_s , which can be expressed as a modulated *comb* function,

$$F_p(\omega) = \sqrt{2\pi} \sum_{s=-\infty}^{+\infty} c_s \delta(\omega - s\Delta\omega). \quad (1.1.11)$$

Some useful properties of the Fourier series expansion are:

- *Parseval's theorem:* If f_p belongs to $L^2([0, \Delta t])$, then

$$\frac{1}{\Delta t} \int_{-\Delta t/2}^{\Delta t/2} |f_p(t)|^2 dt = \sum_{s=-\infty}^{+\infty} |c_s|^2. \quad (1.1.12)$$

- The integral in Eq. (1.1.10) giving the Fourier coefficient c_s can be interpreted as the FT of the time-limited function $f(t) = f_p(t) \text{rect}(t/\Delta t)$, when evaluated at frequencies $s\Delta\omega$, namely $c_s = (\sqrt{2\pi}/\Delta t)F(s\Delta\omega)$. As a consequence,

1. Equation (1.1.11) can be written as $F_p(\omega) = F(\omega) \text{comb}(\omega/\Delta\omega)$.
2. The FT of the time-limited function $f(t)$, when evaluated at frequencies $s\Delta\omega$, is directly proportional to the Fourier coefficients of $f_p(t)$, namely $F(s\Delta\omega) = (\sqrt{2\pi}/\Delta\omega)c_s$. This property is useful when applied to sampled functions, as we will see below.

3. Find the Fourier series expansion of the following periodic functions given in the central *unit cell* $|t| < \Delta t/2$:

- * The squared cosine function $f_p(t) = \cos^2(t)$, with period $\Delta t = \pi$.
- * The rectangle function $f_p(t) = \text{rect}(t)$, with period $\Delta t \geq 1$.

- * The truncated Gaussian function $f_p(t) = \exp[-(t/\tau)^2] \text{rect}(t/\Delta t)$, with period Δt , including the limiting cases $\Delta t \ll \tau$ and $\Delta t \gg \tau$.
- * The Dirac comb function $f_p(t) = \text{comb}(t)$, with period $\Delta t = 1$.

Hint: use the built-in symbol `FourierCoefficient[]` and its option `FourierParameters -> {1, -2π/Δt}` to indicate the period (also `FourierSeries[]` can be used).

4. Plot $f_p(t)$ and its Fourier expansion (1.1.10) by considering a finite but increasing number of Fourier coefficients c_s , for the functions previously analyzed in 3. In each case, plot the list of Fourier coefficients c_s in the range $|s| \leq 10$. Where required, allocate numerical values to the parameters Δt and τ freely.

Hint: use the built-in symbol `ReImPlot[]` for complex-valued functions and `DiscretePlot[]` for the Fourier coefficients.

We may take a step further by sampling the periodic signal $f_p(t)$ at a rate $N/\Delta t$, giving

$$f_p(t) \approx \tilde{f}_p(t) = \frac{\Delta t}{N} \sum_{r=1}^N f(t_r) \delta(t - t_r), \quad \text{and} \quad \tilde{f}_p(t) = \sum_{s=-\infty}^{+\infty} \tilde{c}_s \exp(-is\Delta\omega t), \quad (1.1.13)$$

in the range $0 \leq t < \Delta t$, where $t_r = (r - 1)\Delta t/N$. The periodic function $\tilde{f}_p(t)$ is composed of N Dirac delta functions which are regularly distributed within one period, Δt . Such approach is useful provided that $f_p(t)$ is not itself a finite set of Dirac delta functions within one period, so such cases are disregarded from here on. Some observations can be highlighted:

- The periodic function $f_p(t)$ is approximated to

$$\tilde{f}_p(t) = f_p(t) \text{comb}\left(\frac{t}{\Delta t/N}\right), \quad (1.1.14)$$

which is a comb function of period $\Delta t/N$ modulated by $f_p(t)$ itself.

- Due to the periodicity of $f_p(t)$, equations (1.1.13) and (1.1.14) can be transformed into

$$\tilde{f}_p(t) = \frac{1}{N} \sum_{r=1}^N f_p(t_r) \text{comb}\left(\frac{t - t_r}{\Delta t}\right), \quad (1.1.15)$$

set as a combination of N comb functions of period Δt and mutually shifted by $\Delta t/N$. This can also be inferred by means of the identity $\text{comb}(x/\Delta) = N^{-1} \sum_{s=1}^N \text{comb}[(x - x_s)/N\Delta]$, with $x_s = (s - 1)\Delta$, applied in Eq. (1.1.14).

- The Fourier coefficients of $\tilde{f}_p(t)$ satisfy the recursive relationship $\tilde{c}_{s+N} = \tilde{c}_s$. Consequently, one can find only N independent Fourier coefficients of $\tilde{f}_p(t)$. From here on we will use the set $\{\tilde{c}_0, \tilde{c}_1, \dots, \tilde{c}_{N-1}\}$
- Following Eq. (1.1.11), the FT of $\tilde{f}_p(t)$ yields

$$\tilde{F}_p(\omega) = \frac{\sqrt{2\pi}}{N\Delta\omega} \sum_{s=1}^N \tilde{c}_{s-1} \text{comb}\left(\frac{\omega - \omega_s}{N\Delta\omega}\right), \quad (1.1.16)$$

with $\omega_s = (s - 1)\Delta\omega$, which is also a periodic function with period $N\Delta\omega$. Note that $\tilde{F}_p(\omega)$ is characterized by a finite number N of Fourier coefficients providing the modulation of the N delta functions found within one period.

- Namely, the Fourier coefficients of $\tilde{f}_p(t)$ yield

$$\tilde{c}_{s-1} = \frac{1}{N} \sum_{r=1}^N f_{r-1} \exp \left[\frac{2\pi i(r-1)(s-1)}{N} \right], \quad \text{for } s = \{1, 2, \dots, N\}, \quad (1.1.17)$$

where $f_{r-1} = f(t_r)$. Note that the zeroth-harmonic term appears at position 1 in the resulting list.

Finally, the list of N elements $\mathbf{c} = \{\tilde{c}_0, \tilde{c}_1, \dots, \tilde{c}_{N-1}\}$ can be evaluated by applying the discrete Fourier transform (DFT) to the list $\mathbf{f} = \{f_0, f_1, \dots, f_{N-1}\}$, such that¹ $\mathbf{c} = (1/\sqrt{N})\text{Fourier}[\mathbf{f}]$, where `Fourier[]` is a built-in symbol as defined by default in Mathematica[®].

5. Use the DFT to evaluate the N Fourier coefficients \tilde{c}_s of $\tilde{f}_p(t)$, derived by sampling the periodic functions $f_p(t)$ which were considered in 3. Where required, allocate numerical values to the parameters Δt and τ freely. Employ lists of $N = 2^5$ elements. In addition,
 - Compare these results with the Fourier coefficients c_s of $f_p(t)$, derived analytically in 3, where now $s = \{-\infty, \dots, -2, -1, 0, 1, 2, \dots, +\infty\}$.
 - Discuss if \tilde{c}_{N-1} is closer to either c_{N-1} or c_{-1} . Do the same comparing \tilde{c}_{N-2} with the Fourier coefficients c_{N-2} and c_{-2} . Can you find a more general rule?
 - Discuss the main differences when using $N = 2^6$ elements instead.

Hint: use the built-in symbol `Table[]` to generate a list.

As previously mentioned, a sampled FT of a time-limited signal $f(t)$ of length τ_0 can be obtained by simply replicating such function at different instants in order to generate a periodic function $f_p(t)$ of period $\Delta t \geq \tau_0$, the latter used to subsequently calculate its Fourier coefficients c_s . These coefficients provide $F(\omega)$ at a discrete number of frequencies, which are multiples of the fundamental frequency $\Delta\omega = 2\pi/\Delta t$ (see 2). Namely, $F(s\Delta\omega) = (\sqrt{2\pi}/\Delta\omega)c_s$. Finally, the estimation of c_s is reduced to the (analytically or numerically) evaluation of the integral (1.1.10).

6. Analyze the validity of the approximation $F(\omega_s) \equiv F_{s-1} \approx \tilde{F}_{s-1}$, where \tilde{F}_{s-1} are elements of the list $\mathbf{F} = (\sqrt{2\pi}/\Delta\omega)\mathbf{c}$ for $s = \{1, 2, \dots, N\}$, and $\omega_s = (s-1)\Delta\omega$. Note that $\tilde{F}_{s+N} = \tilde{F}_s$. For that purpose:
 - Show that this problem is equivalent to comparing the Fourier transform of $f_p(t)$, which can be set as $F_p(\omega) = F(\omega) \text{comb}(\omega/\Delta\omega)$, and $\tilde{F}_p(\omega)$ given in Eq. (1.1.16).
Hint: use the identity $\text{comb}(\omega/\Delta\omega) = N^{-1} \sum_{s=1}^N \text{comb}[(\omega - \omega_s)/N\Delta\omega]$.
 - Use the DFT to evaluate the N elements of \mathbf{F} , derived by sampling the functions $f(t)$ which were considered in 1 at a rate $N/\Delta t$. Where required, allocate numerical values to the parameters τ , Δt , and ω_0 freely. Disregard cases involving Dirac delta functions. Employ lists of $N = 2^5$ elements.
 - Compare these results with the Fourier transforms $F(\omega)$ derived analytically in 1, when evaluated at frequencies $\omega_s = (s-1)\Delta\omega$, where now $s = \{-\infty, \dots, -2, -1, 0, 1, 2, \dots, +\infty\}$. In particular, discuss if \tilde{F}_{N-1} is closer to either F_{N-1} or F_{-1} . Do the same comparing \tilde{F}_{N-2} with F_{N-2} and F_{-2} . Can you find a more general rule?

¹Other definitions of the DFT are used in some scientific and technical fields.

- Using a given time-limited function $f(t)$ within the working range $|t| \leq \Delta t/2$, is there any improvement in the DFT-based estimation of the FT by using $N = 2^6$ elements? And using $N = 2^7$ elements? Note that the length Δt of the working range is kept fixed but the sampling rate is being doubled in each step.
- Compare the accuracy of the DFT obtained for a given time-limited function $f(t)$ within the working range $|t| \leq \Delta t/2$ when using $N = 2^5$ points, with the DFT of the same function but doubling the length of the working range to $2\Delta t$, by applying a zero padding in the range $\Delta t/2 < |t| \leq \Delta t$, and also doubling the number of points to $2N = 2^6$. Note that the sampling rate $N/\Delta t$ is conserved in both cases.
- Plot the lists \mathbf{F} and $F(\omega_s)$ for all the functions previously analyzed.

Hint: consider using the built-in symbol `RotateLeft[list, len/2]`, where $len = \text{Length}[list]$, to swaps the left and right halves of $list$. The latter serves to transform \mathbf{F} into the list $\{\tilde{F}_{-N/2}, \tilde{F}_{-N/2+1}, \dots, \tilde{F}_{-1}, \tilde{F}_0, \tilde{F}_1, \dots, \tilde{F}_{N/2-1}\}$, leaving \tilde{F}_0 in the center of the list.

1.2 Interference by division of wavefront

Introductory notes: rotation of plane waves

Consider a monochromatic plane wave of time frequency ω propagating in free space. The analytic representation of the electric field can be written as $\vec{E}(\vec{r}, t) = \hat{\sigma} E_0 \exp(i\vec{k} \cdot \vec{r} - i\omega t)$, where $\hat{\sigma}$ is a unit vector ($\hat{\sigma} \cdot \hat{\sigma}^* = 1$) characterizing its state of polarization, E_0 is the complex-valued amplitude of the electric field measured in V/m, $\vec{k} = k\hat{q}$ is the wave vector, $\hat{q} \cdot \hat{q}^* = 1$, $k = \omega/c$ is the wavenumber, and $c = 1/\sqrt{\epsilon_0\mu_0}$ is the speed of light in vacuum. Note that:

1. The electric field is a transverse wave, i.e. $\hat{q} \cdot \hat{\sigma} = 0$. In other words, $\vec{E} \perp \vec{k}$.
2. The magnetic field of the plane wave can be set as $\vec{H}(\vec{r}, t) = \hat{\pi} H_0 \exp(i\vec{k} \cdot \vec{r} - i\omega t)$, provided that the unit vector $\hat{\pi} = \hat{q} \times \hat{\sigma}$ and the amplitude of the magnetic field $H_0 = E_0/Z_0$, where $Z_0 = \sqrt{\mu_0/\epsilon_0}$ ($\approx 376.7 \Omega$) is the intrinsic impedance of free space.
3. Using the fact that the rotation of a vector \vec{x} by an angle θ around the axis characterized by the unit vector \hat{u} can be written as²

$$R_u(\theta)\vec{x} = \hat{u}(\hat{u} \cdot \vec{x}) + \cos(\theta)(\hat{u} \times \vec{x}) \times \hat{u} + \sin(\theta)(\hat{u} \times \vec{x}),$$

the electric field and magnetic field of the plane wave given above can satisfy Maxwell's equations under the rotational transformations $R_{\hat{u}}(\theta)\vec{k}$, $R_{\hat{u}}(\theta)\hat{\sigma}$, and $R_{\hat{u}}(\theta)\hat{\pi}$, applied simultaneously, and occurring independently of the orientation of the rotation unit vector \hat{u} .

Note: in Mathematica[®], one may use `RotationMatrix[θ , { u_x, u_y, u_z }]` to generate a 3D rotation matrix equivalent to $R_u(\theta)$.

4. A generalization of **3** can be established when the rotation is described by the multiplication matrix $R = R_z(\alpha) R_y(\beta) R_x(\gamma)$, whose yaw, pitch, and roll angles are α , β and γ , respectively, which is applied to the vectors \vec{k} , $\hat{\sigma}$, and $\hat{\pi}$ characterizing an electromagnetic plane wave.

1.2.1 Interference of two plane waves

First, consider an optical plane wave whose electric field is $\mathbf{E}(\vec{r}, t) = \text{Re}[\vec{E}(\vec{r}, t)]$, where $\vec{E}(\vec{r}, t) = \hat{\sigma} E_0 \exp(i\vec{k} \cdot \vec{r} - i\omega t)$, which propagates along the z -axis ($\hat{q} = \hat{z}$) in free space ($k = \omega/c$), having a wavenumber $k = 4\pi \mu\text{m}^{-1}$ ($\lambda = 0.5 \mu\text{m}$), an amplitude $E_0 = 1 \text{ V/m}$, and a state of polarization characterized by the unit vector $\hat{\sigma} = \hat{y}$, i.e. the plane wave is linearly polarized.

1. Plot the time evolution of the electric field $\mathbf{E}(\vec{r}, t)$ at different points of the 3-D domain Ω_3 , given by $|x| \leq \lambda$, $|y| \leq \lambda$, and $0 \leq z \leq 2\lambda$. Show that the electric field vector executes a simple-harmonic oscillation of period $T = \lambda/c$ ($T = 1.67 \text{ fs}$ in our case) along the y axis.
Hint: use `VectorPlot3D[]` to show $\mathbf{E}(\vec{r}, t)$ in a given instant t within Ω , and `Animate[]` in $0 \leq t \leq T$ to represent its time evolution.

2. Plot the time evolution of the energy density, $U(\vec{r}, t) = U_e(\vec{r}, t) + U_m(\vec{r}, t)$, where

$$U_e(\vec{r}, t) = \frac{1}{2}\epsilon_0\mathbf{E} \cdot \mathbf{E}, \quad \text{and} \quad U_m(\vec{r}, t) = \frac{1}{2}\mu_0\mathbf{H} \cdot \mathbf{H},$$

where $\mathbf{H}(\vec{r}, t) = \text{Re}[\vec{H}(\vec{r}, t)]$ (see [introductory notes](#)), and the Poynting vector,

$$\mathbf{S}(\vec{r}, t) = \mathbf{E} \times \mathbf{H},$$

²https://en.wikipedia.org/wiki/Rotation_matrix

in points of Ω_3 . Show that they exhibit a periodic oscillation of period $T/2$. Finally, show that one can set $\mathbf{S}(\vec{r}, t) = S_z(z, t)\hat{z}$, and plot $S_z(z, t)$ in $0 \leq z \leq 2\lambda$.

Hint: use `ContourPlot[]` to represent scalar fields such as $U(\vec{r}, t)$ in different planes ($y = 0$, for instance) within Ω_3 .

3. Show that the time-averaged energy density, defined as

$$w(\vec{r}) = \frac{1}{T} \int_0^T U(\vec{r}, t) dt = \frac{1}{4} \epsilon_0 \vec{E} \cdot \vec{E}^* + \frac{1}{4} \mu_0 \vec{H} \cdot \vec{H}^*,$$

leads to a uniform pattern, $w(\vec{r}) = w_0$, where $w_0 = \epsilon_0 |E_0|^2 / 2$. Also show that the time-averaged Poynting vector, which is determined by the real part of the complex Poynting vector

$$\vec{S}(\vec{r}) = \frac{1}{2} \vec{E} \times \vec{H}^*,$$

yields the vector $S_0 \hat{q}$ at every point of the space, where the intensity $S_0 = w_0 c = |E_0|^2 / (2Z_0)$.

4. Next, consider that the plane wave of electric field $\vec{E}(\vec{r}, t)$ is split into two identical plane waves of amplitude $E_0/2$ each one, giving $\vec{E}_1 = \vec{E}_2 = \vec{E}/2$. By optical means, the electric field $\vec{E}_1(\vec{r}, t)$ is transformed into $\vec{E}'_1(\vec{r}, t)$ by a rotation $R_y(\beta_0)$ in the terms given in the [introductory notes](#) (see [3](#)), where the pitch angle $\beta_0 = \pi/4$. However the electric field $\vec{E}_2(\vec{r}, t)$ is transformed into $\vec{E}'_2(\vec{r}, t)$ by a rotation $R_y(-\beta_0)$. Finally, consider the interference of the rotated wave fields, $\vec{E}'(\vec{r}, t) = \vec{E}'_1(\vec{r}, t) + \vec{E}'_2(\vec{r}, t)$, occurring in the region of interest.

- Plot the time evolution of the electric field, $\mathbf{E}'(\vec{r}, t) = \text{Re}[\vec{E}'(\vec{r}, t)]$, determined at points in Ω_3 . Show that the wave field is periodic along the x axis with a spatial period $p_x = \lambda / \sin(\beta_0)$, however it is invariant under translations along the y axis. Analyze the state of polarization at the observed points in Ω_3 . Finally, plot the time evolution of the y component of the electric field, $\hat{y} \cdot \mathbf{E}'(\vec{r}, t)$, in the 2-D domain Ω_2 given by $|x| \leq p_x$ and $0 \leq z \leq 2\lambda$.
 - Plot the time evolution of the energy density of the superposition of these two polarized plane waves at points of Ω_2 . Plot the Poynting vector at points of Ω_3 . Show that they exhibit a time-domain oscillation of period $T/2$. Show that one can set $\mathbf{S}(\vec{r}, t) = S_x(x, z, t)\hat{x} + S_z(x, z, t)\hat{z}$, and plot $\mathbf{S}(\vec{r}, t)$ in Ω_2 . Is there any periodicity of the evaluated patterns along the x axis? And along the z axis?
Hint: use `ContourPlot[]` to represent the scalar field $U(\vec{r}, t)$ within Ω_2 . Use `VectorPlot[]` to represent the vector field $\mathbf{S}(\vec{r}, t)$ in Ω_2 .
 - Plot the time-averaged energy density in Ω_2 and the time-averaged Poynting vector at points of either Ω_2 or Ω_3 . Show that one can set $w(\vec{r}) = w_0 [\cos^2(\beta_0) \cos^2(2\pi x/p_x) + \sin^2(\beta_0)/2]$ and $\text{Re}(\vec{S}) = S_0 \cos(\beta_0) \cos^2(2\pi x/p_x) \hat{z}$, the latter describing the *Young fringes* pattern.
5. Repeat [4](#) but considering the interference of two plane waves with initial (prior to the application of rotation) state of polarization given by the unit vector $\hat{\sigma} = \hat{x}$. In addition, consider wave rotations of pitch angle: (a) $\beta_0 = \pi/4$, and (b) $\beta_0 = \pi/2$. Here, one may plot the time evolution of the x and z components of the electric field in Ω_2 , simultaneously.
6. Repeat [4](#) but considering the interference of two plane waves with original state of polarization given by the unit vector $\hat{\sigma} = (\hat{x} + i\hat{y})/\sqrt{2}$. In addition, consider a pitch angle $\beta_0 = \pi/4$.

1.2.2 Periodic interference patterns (optional)

First, consider an optical plane wave whose electric field is $\vec{E}(\vec{r}, t) = \hat{\sigma} E_0 \exp(i\vec{k} \cdot \vec{r} - i\omega t)$, which propagates along the z -axis ($\hat{q} = \hat{z}$) in free space ($k = \omega/c$), having a wavenumber $k = 4\pi \mu\text{m}^{-1}$ ($\lambda = 0.5 \mu\text{m}$), an amplitude $E_0 = 1 \text{ V/m}$, and a state of polarization characterized by the unit vector $\hat{\sigma} = \hat{y}$, i.e. the plane wave is linearly polarized.

Next, consider that the plane wave of electric field $\vec{E}(\vec{r}, t)$ is split into an odd number $M = 3$ of identical plane waves with amplitude E_0/M each one, giving wavelets of electric field $\vec{E}_m = \vec{E}/M$, with $m = 0, \pm 1, \dots, (M-1)/2$. By optical means, the electric field $\vec{E}_1(\vec{r}, t)$ of one wavelet is transformed into $\vec{E}'_1(\vec{r}, t)$ by a rotation $R_y(\beta_0)$ in the terms given in the **introductory notes** (see **3**), where the pitch angle $\beta_0 = \pi/18$. The electric field $\vec{E}_{-1}(\vec{r}, t)$ is transformed into $\vec{E}'_{-1}(\vec{r}, t)$ by a mirror-symmetric transformation $R_y(-\beta_0)$. In general, the electric field $\vec{E}_m(\vec{r}, t)$ of the m -th wavelet is transformed into $\vec{E}'_m(\vec{r}, t)$ by the rotation $R_y(\beta_m)$, provided that

$$\sin(\beta_m) = m \sin(\beta_0), \quad (1.2.1)$$

and $|\beta_m| \leq \pi/2$. Finally, consider the interference of the rotated wave fields, $\vec{E}'(\vec{r}, t) = \sum_m \vec{E}'_m(\vec{r}, t)$, occurring in the region of interest.

1. Show that the electric field satisfies the following periodicity property:

$$\vec{E}'(x + p_x, y, z, t) = \vec{E}'(x, y, z, t),$$

where $p_x = \lambda/\sin\beta_0$ is the period along the x axis. Show that the electric field is invariant under translations in the spatial coordinate y .

Note: Equation **1.2.1** becomes $\sin(\beta_m) = m\lambda/p_x$, which is formally equivalent to the *grating equation* when light is normally incident on the grating.

2. Plot the time evolution of the electric field, $\text{Re}[\vec{E}'(\vec{r}, t)]$, determined at different points of the plane $z = 0$, provided that $|x| \leq 2p_x$. Furthermore, analyze the state of polarization at the observed points of the xy plane.
3. Plot the time-averaged energy density and the time-averaged Poynting vector at different points of the plane $z = 0$.
4. Repeat **2-3** but considering the interference of: (a) $M = 5$, and (b) $M = 7$ plane waves with initial state of polarization given by the unit vector $\hat{\sigma} = \hat{y}$.
5. Find the maximum number (M_{max}) of plane waves to interfere under the restriction $|m| \leq 1/\sin(\beta_0)$, which can be derived from $|\sin(\beta_m)| \leq 1$. Furthermore, repeat **2-3** but considering the interference of M_{max} plane waves with initial state of polarization given by the unit vector $\hat{\sigma} = \hat{y}$.
6. Repeat **2-4** but considering the interference of plane waves with initial state of polarization given by the unit vector $\hat{\sigma} = (\hat{x} + \hat{y})/\sqrt{2}$.

1.3 Interference by division of amplitude

Introductory notes: Scattered fields in 1-D domains under normal incidence

Consider a semi-space $z < 0$ filled with an isotropic homogeneous material of index of refraction n_1 , which is real valued and positive for convenience. In $z > L$ (with $L > 0$) the medium is isotropic and homogeneous with index of refraction n_2 , which is not necessarily real valued ($\text{Im}(n_2) \geq 0$ is always imposed). In the intermediate space, $0 < z < L$, the medium is inhomogeneous with index of refraction $n(z)$. Finally, the photonic systems is free of charges and currents.

1. In $z < 0$, a 1-D time-harmonic electric field $\vec{E}(z) = \hat{\sigma}E(z)\exp(-i\omega t)$ satisfies the Helmholtz equation, $[\partial_z^2 + k_0^2 n_1^2]E(z) = 0$, where $k_0 = \omega/c$ is the wavenumber in a vacuum, and $\hat{\sigma}$ is a complex, unitary ($\hat{\sigma} \cdot \hat{\sigma}^* = 1$), transverse ($\hat{\sigma} \cdot \hat{z} = 0$) vector denoting the state of polarization of the wave field. In addition, its magnetic field $\vec{H}(z) = \hat{\pi}H(z)\exp(-i\omega t)$ can be determined by means of $H(z) = (ik_0 Z_0)^{-1} \partial_z E(z)$, where $Z_0 = (\mu_0/\epsilon_0)^{1/2}$ is the intrinsic impedance in free space, and $\hat{\pi} = \hat{z} \times \hat{\sigma}$.
 - (a) Furthermore, $E(z) = E_0 [\exp(ik_1 z) + r \exp(-ik_1 z)]$ is a solution of the 1-D Helmholtz equation in $z < 0$, E_0 and r are complex-valued constants, and $k_1 = k_0 n_1$ is the wave number in the medium. In fact, r is the reflection coefficient, which can be estimated by means of $r = \frac{E(0)}{E_0} - 1$, and $R = |r|^2$ gives its reflectance. Finally, the magnetic field is set as $H(z) = n_1 H_0 [\exp(ik_1 z) - r \exp(-ik_1 z)]$, where $H_0 = E_0/Z_0$ is its amplitude.
 - (b) The complex Poynting vector, $\vec{S}(z) = \frac{1}{2} \vec{E}(z) \times \vec{H}^*(z) = \hat{z} S_z(z)$, has its real part at the boundary $z = 0$ given by $\text{Re}[S_z(0)] = n_1 S_0 (1 - |r|^2)$, where the intensity $S_0 = \frac{1}{2} |E_0|^2 / Z_0$.
 - (c) The electric field in $z \leq 0$ satisfies the boundary condition $[ik_1 E(z) + \partial_z E(z)]_{z=z_1} = 2ik_1 E_0 \exp(ik_1 z_1)$, which can be applied at a transverse plane $z = z_1$ with $z_1 \leq 0$.
2. In $z > L$, the 1-D electric field satisfies the Helmholtz equation, $[\partial_z^2 + k_2^2] \vec{E}(z) = 0$, where $k_2 = k_0 n_2$. Note that, in general, k_2 is complex valued, and $\text{Im}(k_2) \geq 0$ always occurs.
 - (a) One find the solution $E(z) = E_0 t \exp[ik_2(z - L)]$ to the Helmholtz equation in $z > L$, where $\vec{E}(z) = \hat{\sigma}E(z)$, and $\hat{\sigma}$ represents the same state of polarization of the incident and reflected fields. Here, t is the transmission coefficient, which can be estimated by $t = \frac{E(L)}{E_0}$. Also, the magnetic field $\vec{H}(z) = \hat{\pi}H(z)$, where $H(z) = n_2 H_0 t [ik_2(z - L)]$.
 - (b) The complex Poynting vector yields $\text{Re}[\vec{S}(z)] = \text{Re}[\vec{S}(L)] \exp[-2\text{Im}(k_2)(z - L)]$, if $z > L$, where $\text{Re}[\vec{S}(L)] = \hat{z} S_0 |t|^2 \text{Re}(n_2)$. Thus, $T = |t|^2 \text{Re}(n_2)/n_1$ gives the optical transmittance.
 - (c) In $z \geq L$, the electric field satisfies the *radiation condition*, $[ik_2 E(z) - \partial_z E(z)]_{z=z_2} = 0$, which is established at any transverse plane $z = z_2$ provided that $z_2 \geq L$.
3. In the stratified medium, $0 < z < L$, the electric field $\vec{E}(z) = \hat{\sigma}E(z)$ satisfies the equation,

$$\left[\frac{\partial^2}{\partial z^2} + k_0^2 n^2(z) \right] E(z) = 0, \quad (1.3.1)$$

for an arbitrary state of polarization $\hat{\sigma}$ of the incident wave field. In addition:

- (a) The magnetic field can be evaluated as $\vec{H}(z) = \hat{\pi}H(z)$, where $H(z) = (i\omega\mu_0)^{-1} \partial_z E(z)$.

- (b) Continuity of $E(z)$ and $\partial_z E(z)$ can be used as boundary conditions under the presence of discontinuities of the index of refraction $n(z)$.
- (c) For instance, assuming a homogeneous scattering layer, where $n(z) = n_L$:

- One finds the solution to the Helmholtz equation (1.3.1) as follows,

$$E(z) = E_0 [t_L \exp(ik_L z) + r_L \exp(-ik_L z)], \quad 0 < z < L. \quad (1.3.2)$$

Here, $k_L = k_0 n_L$, and t_L and r_L are complex-valued constants.

- One may show the validity of the *Airy's formulae* given as [2, section 4.2]

$$r = \frac{r_{1L} + r_{L2} \exp(2ik_L L)}{1 - r_{L1} r_{L2} \exp(2ik_L L)}. \quad (1.3.3)$$

$$t = \frac{t_{1L} t_{L2} \exp(ik_L L)}{1 - r_{L1} r_{L2} \exp(2ik_L L)}, \quad (1.3.4)$$

$$t_L = \frac{t_{1L}}{1 - r_{L1} r_{L2} \exp(2ik_L L)}, \quad (1.3.5)$$

$$r_L = \frac{t_{1L} r_{L2} \exp(2ik_L L)}{1 - r_{L1} r_{L2} \exp(2ik_L L)}, \quad (1.3.6)$$

where the *Fresnel transmission* and *reflection coefficients* are given by

$$r_{\alpha\beta} = \frac{n_\alpha - n_\beta}{n_\alpha + n_\beta} = -r_{\beta\alpha}, \quad (1.3.7)$$

$$t_{\alpha\beta} = \frac{2n_\alpha}{n_\alpha + n_\beta} = 1 + r_{\alpha\beta}. \quad (1.3.8)$$

- (d) By applying Poynting's theorem in the stratified medium, $\text{Re}[S_z(0)] - \text{Re}[S_z(L)] = n_1 S_0 A$, one finds the optical absorbance $A = 1 - T - R$.

1.3.1 Antireflection coatings

An *antireflection coating* can be used to completely eliminate the reflection of light appearing at a flat interface between two media of distinct indices of refraction, $n_1 \neq n_2$ [2, sections 4.4.1 and 7.3]. It consists of a quarter-wave layer ($k_L L = \pi/2$) set in $0 < z < L$, with $n(z) = n_L$ satisfying $n_L^2 = n_1 n_2$.

1. Show that $r_{1L} = r_{L2}$ in an antireflection coating and, therefore, the reflection coefficient r given in Eq. (1.3.3) vanishes.

For numerical purposes, set the amplitude $E_0 = 1$ V/m, and the vacuum wavelength $\lambda_0 = 500$ nm which the antireflection coating is designed for. Here, $n(z) = n_1$ within $z_1 \leq z < 0$, and $n(z) = n_2$ within $L < z \leq z_2$. Firstly use $n_1 = 1$ and $n_2 = 1.5$. Also set the input and output ports at $z_2 = -z_1 = 2\lambda_0$.

2. Evaluate the index of refraction n_L and the layer width L of our antireflection coating.
3. Find numerically the solution to the Helmholtz equation (1.3.1) within the whole interval $z_1 \leq z \leq z_2$, providing the z dependence of the electric field, $E(z)$. Apply the Robin boundary condition (1.1.5) at the input port, and the radiation condition (1.1.6) at the output port.

4. Plot the real and imaginary part of the wave function $E(z)$ (or $u(x)$, see 2) which was found previously. Also plot $|E(z)|$ within the region of computation.
5. Repeat 3–4 for the boundary wavelengths in the visible, $\lambda_0 = 390$ nm and $\lambda_0 = 780$ nm, but keeping the layer width L (and n_L) as evaluated in 2 for $\lambda_0 = 500$ nm. In addition, calculate the optical reflectance $R = |r|^2$, both numerically and using Eq. (1.3.3), at both boundary wavelengths.
6. Repeat 3–4 for an antireflection coating of width: (a) $L + \lambda_0/(2n_L)$, and (b) $L + \lambda_0/n_L$, where $L = \lambda_0/(4n_L)$ and $\lambda_0 = 500$ nm. Discuss these results.
7. Repeat 3–4 considering an antireflection coating made of magnesium fluoride ($n_L = 1.38$), which is a frequently-used low-index film. Also, calculate the optical reflectance R , both numerically and using Eq. (1.3.3).

1.3.2 Optical tunneling in ultrathin metal films

It is known that thin films of noble metals have a maximum optical transmittance in the shorter part of spectrum. This can be in practice used to observe the *optical tunneling effect* under normal incidence. It occurs setting in $0 < z < L$ a layer of index of refraction $n(z) = n_L$, provided that $\text{Re}(n_L^2) < 0$ and $k_0L \ll 1$. In all cases, transmittance of thin metal films decreases with increasing film thickness L .

For numerical purposes, consider a silver layer of index of refraction $n_L = 0.055 + i4.0$ at $\lambda_0 = 600$ nm, deposited on a glass substrate of index $n_2 = 1.5$ and immersed in air ($n_1 = 1$). Again, set the amplitude $E_0 = 1$ V/m, and the input and output ports are located at $z_2 = -z_1 = 2\lambda_0$.

1. Find numerically the solution to the Helmholtz equation (1.3.1) within the whole interval $z_1 \leq z \leq z_2$, providing the z dependence of the electric field, $E(z)$. Consider a metal layer of thickness $L = 20$ nm. Apply the Robin boundary condition (1.1.5) at the input port, and the radiation condition (1.1.6) at the output port.
2. Plot the real and imaginary part of the wave function $E(z)$ (or $u(x)$, see 2) which was found previously. Also plot $|E(z)|$ within the region of computation. In addition, calculate the optical reflectance R , transmittance T , and absorbance A , both numerically and using Eq. (1.3.3).
3. Repeat 1–2 for a silver layer of thickness: (a) $L = 50$ nm, (b) $L = 100$ nm, (c) $L = 200$ nm, and (d) $L = \lambda_0$.
Hint: higher accuracy and precision goals may give a different result for long lengths L , and increasing the goals extends the correct solution further; thus include the following options in `NDSolve[]`: `AccuracyGoal -> 20`, `PrecisionGoal -> 20`, `WorkingPrecision -> 35`.
4. Plot R , T , and A as a function of L , derived from Eq. (1.3.3).

1.4 Diffraction

Introductory notes: diffraction in the paraxial regime

Electromagnetic fields in an isotropic homogeneous medium of index of refraction $n > 0$ are governed in general by the scalar Helmholtz equation $(\nabla^2 + k^2)E(x, y, z) = 0$, where $E(x, y, z)$ is the analytic representation of a (scalar) field distribution that is harmonic in time as $\exp(-i\omega t)$, and $k = n\omega/c \equiv 2\pi/\lambda$.

In the paraxial regime around the z axis, it is convenient to extract the primary $\exp(ikz)$ propagation factor out of E , by writing $E(x, y, z) \equiv u(x, y, z) \exp(ikz)$. The slowly varying dependence of $u(x, y, z)$ on z , considered under the so-called *slowly varying envelope approximation*, can be expressed mathematically by the paraxial Helmholtz equation [3, chapter 16],

$$\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + i2k \frac{\partial u}{\partial z} = 0, \quad (1.4.1)$$

which is valid provided that $|\partial_z^2 u| \ll |2k\partial_z u|$.

A solution to Eq. (1.4.1) can be set by means of Huygens' integral equation in the Fresnel approximation,

$$u(x, y, z) = \frac{1}{i\lambda z} \iint_{-\infty}^{+\infty} u_0(x_0, y_0) \exp \left\{ \frac{ik}{2z} [(x - x_0)^2 + (y - y_0)^2] \right\} dx_0 dy_0, \quad (1.4.2)$$

where $u_0(x, y) = u(x, y, 0)$ represents the wave field u evaluated at the reference plane $z = 0$. Equation (1.4.2) is also known as the *Huygens-Fresnel diffraction integral*, and is useful for the evaluation of diffracted fields by an aperture placed at $z = 0$. If the aperture has an amplitude transmittance $t(x, y)$ and is illuminated by a normally-incident plane wave of amplitude E_0 at $z = 0$, one can set $u_0(x, y) = E_0 t(x, y)$ when applying the *Kirchhoff boundary conditions*.

Note that Huygens-Fresnel diffraction integral given in (1.4.2) can be set as a 2-D convolution, $u(x, y, z) = (u_0 \otimes h_z)(x, y)$, where the impulse response $h_z(x, y) = h_z(x)h_z(y)$ and

$$h_z(x) = (i\lambda z)^{-1/2} \exp [ikx^2/(2z)].$$

As a consequence, one can use the properties of the Fourier transform, taking into account that $\mathcal{F}(h_z)(q_x, q_y) = H_z(q_x, q_y) = H_z(q_x)H_z(q_y)$, where $H_z(q_x) = (2\pi)^{-1/2} \exp [-izq_x^2/(2k)]$ (see 1.1.3).

Assuming that the wave function u_0 is invariant under translations along the y axis leading to $u_0(x, y) \equiv u_0(x)$, as we will do from here on, the diffracted fields in a plane $z \neq 0$ are also invariant under translations along the y axis, and therefore we may write $u(x, y, z) \equiv u(x, z)$. In this case, the paraxial Helmholtz equation (1.4.1) yields $(\partial_x^2 + i2k\partial_z)u(x, z) = 0$. Furthermore, Huygens' diffraction integral (1.4.2) is reduced to $u(x, z) = (u_0 \otimes h_z)(x)$. As mentioned before, the properties of the Fourier transform allow us to evaluate the diffracted wave fields as

$$u(x, z) = \mathcal{F} \left\{ U_0(q_x) \exp [-izq_x^2/(2k)] \right\} (-x), \quad (1.4.3)$$

where $U_0(q_x) = \mathcal{F}(u_0)(q_x)$. This method is efficient when applied sufficiently near the reference plane, that is, for the evaluation of the so-called *near field* within $0 \leq z \leq z_1$, where $z_1 = 2k/q_{\max}^2$ provided that $|U_0(q_x)|$ reaches significant values in the spectral band $|q_x| \leq q_{\max}$.

On another note, using the definition of the Fourier transform given in Eq. (1.1.9), Huygens' diffraction integral can also be set as

$$u(x, z) = \sqrt{2\pi} h_z(x) F_z(q_x), \quad (1.4.4)$$

where $F_z(q_x) = \mathcal{F}(f_z)(q_x)$ is the 1-D Fourier transform of the wave function

$$f_z(x) = u_0(x) \exp[ikx^2/(2z)],$$

provided that the spatial frequency $q_x = -kx/z$. This method is efficient when applied sufficiently far from the reference plane, $z \geq z_2$, with $z_2 = kx_{\max}^2/2$ provided that $|u_0(x)|$ reaches significant values in the range $|x| \leq x_{\max}$. In the *far field* ($z \gg z_2$) one can observe the *Fraunhofer diffraction pattern*, which is evaluated by using the approximation $f_z(x) \rightarrow u_0(x)$.

Typically, one may find that q_{\max} is of the order of $2/x_{\max}$, yielding $z_1 \approx z_2$ that is a distance sometimes called *Rayleigh range*. In this context, diffraction equations can be conveniently rewritten in terms of normalized spatial coordinates $\xi = x/x_{\max}$ and $\zeta = z/z_R$, where $z_R = kx_{\max}^2/2$ is the Rayleigh range. For instance, the 1-D paraxial wave equation yields

$$(\partial_\xi^2 + 4i\partial_\zeta) \tilde{u}(\xi, \zeta) = 0, \quad (1.4.5)$$

where $u(x, z) = E_0 \tilde{u}(\xi, \zeta)$. Similarly, equation (1.4.3) becomes

$$\tilde{u}(\xi, \zeta) = \mathcal{F}\{\tilde{U}(q_\xi, 0) \exp(-i\zeta q_\xi^2/4)\}(-\xi), \quad (1.4.6)$$

where $q_\xi = x_{\max} q_x$. Finally, equation (1.4.4) becomes

$$\tilde{u}(\xi, \zeta) = (i\zeta/2)^{-1/2} \exp(i\xi^2/\zeta) \mathcal{F}(\tilde{f}_\zeta)(q_\xi), \quad \text{with} \quad \tilde{f}_\zeta(\xi) = \tilde{u}(\xi, 0) \exp(i\xi^2/\zeta), \quad (1.4.7)$$

and $q_\xi = -2\xi/\zeta$.

1.4.1 Diffraction gratings: Talbot effect

Consider a 1-D diffraction grating characterized by an amplitude transmittance $t(x)$, which is illuminated by a normally-incident plane wave of amplitude E_0 at $z = 0$. The transmittance function has a period Δx , i.e. $t(x + \Delta x) = t(x)$, and can be set in Fourier series expansion [see Eq. (1.1.10)], where c_s is the Fourier coefficient of its s -th harmonic. Typically, the fundamental spatial frequency $\Delta q_x = 2\pi/\Delta x$ of a diffraction grating is conveniently given in lines per centimeter.

1. Show that the field $u(x, z)$, evaluated by means of Eqs. (1.4.3) and (1.1.11), can be set as

$$u(x, z) = E_0 \sum_{s=-\infty}^{+\infty} c_s \exp[-i2\pi s(x/\Delta x)] \exp[-i2\pi s^2(z/z_T)], \quad (1.4.8)$$

where $z_T = 2(\Delta x)^2/\lambda$ is the *Talbot length*. In addition:

- Show that $u(x, z_T) = u(x, 0) = E_0 t(x)$. Therefore, the wave field of a light diffracting through a grating is periodically reproduced, with a period given by the Talbot length.³
 - Show that $u(x, z_T/2) = E_0 t(x + \Delta x/2)$. At half the Talbot length, a self-image also occurs, but laterally shifted by half the width of the grating period.
2. Calculate the Fourier coefficients c_s of the transmittance function $t(x)$ given in $|x| < \Delta/2$, characterizing the following 1-D diffraction gratings of period Δx :
 - The *square-wave amplitude grating* composed of evenly spaced parallel slits, giving $t(x) = \text{rect}(x/w)$, where $w \leq \Delta x$ is the slit width.

³https://en.wikipedia.org/wiki/Talbot_effect

- The *sinusoidal phase grating* with $t(x) = \exp[i\varphi_0 \sin(\Delta q_x x)]$, where φ_0 represents the peak excursion of the sinusoidal phase variation.
- The *square-wave phase grating* with transmittance function $t(x) = 1 - [1 - \exp(i\varphi_0)] \text{rect}(x/w)$.
- The *blazed grating* with ‘saw tooth’ phase profile, giving $t(x) = \exp(i\varphi_0 x/\Delta x)$.

Hint: When analytical expressions of c_s cannot be found, use the DFT to find them numerically, namely \tilde{c}_s , as analyzed in 5.

3. Plot the normalized diffraction pattern $|u(x, z)|^2$ of the transmission gratings analyzed above, using Eq. (1.4.8) within the range $|x| \leq \Delta x/2$ and $0 \leq z \leq z_T$. For numerical purposes, use: (1) $E_0 = 1$, (2) $w = \Delta/2$, (3) $\varphi_0 = 1.84$ rads for the sinusoidal phase grating, $\varphi_0 = \pi$ for the square-wave phase grating, and $\varphi_0 = \{\pm\pi, \pm 2\pi\}$ for the blazed grating. Also plot the field $\text{Re}[u(x, z)]$ for phase gratings. Take an even number N of Fourier harmonics, ranging from the $(-N/2)$ -th to the $(+N/2 - 1)$ -th order, and show that accuracy of the estimated wave fields increases as long as the parameter

$$\eta = \frac{\sum_{s=-N/2}^{+N/2-1} |c_s|^2}{\frac{1}{\Delta x} \int_{-\Delta x/2}^{\Delta x/2} |t(x)|^2 dx} \quad (1.4.9)$$

approaches to unity, as inferred from Parseval’s theorem (1.1.12).

Hint: use normalized spatial coordinates $\xi = x/\Delta x$ and $\zeta = z/z_T$. Note that using $N > 32$ in the proposed method may result in a time-consuming computation.

1.4.2 Diffraction by a slit

Consider a slit characterized by a transmittance function $t(x) = \text{rect}(x/w)$, where w is the slit width. Consider a monochromatic plane wave propagating in free space, which electric field $\vec{E}(z, t) = \hat{x}E_0 \exp(ikz - i\omega t)$, where the wavenumber $k = 2\pi/\lambda$ and E_0 denotes a field amplitude. By setting the slit at $z = 0$, the diffracted field within the paraxial approximation $u(x, z) = E_0 \tilde{u}(\xi, \zeta)$, where [3, chapter 18]

$$\tilde{u}(\xi, \zeta) = \frac{1}{2} \left[\text{erf} \left(\frac{\xi + \frac{1}{2}}{\sqrt{i\zeta}} \right) - \text{erf} \left(\frac{\xi - \frac{1}{2}}{\sqrt{i\zeta}} \right) \right], \quad \zeta > 0. \quad (1.4.10)$$

Here, $\xi = x/w$ and $\zeta = z/z_R$ are normalized spatial coordinates, $z_R = kw^2/2$ is the *Rayleigh range*, and $\text{erf}(\tau) = 2\pi^{-1/2} \int_0^\tau \exp(-t^2) dt$ is the error function.

1. Show the validity of Eq. (1.4.10) by means of Eq. (1.4.6).
Hint: use $\tilde{u}(\xi, 0) = \text{rect}(\xi)$ and $\tilde{U}(q_\xi, 0) = (2\pi)^{-1/2} \text{sinc}(q_\xi/2)$.
2. Plot the normalized intensity patterns $|\tilde{u}(\xi, \zeta)|^2$ at planes $\zeta = 1/(4\pi N_F)$ within the range $|\xi| \leq 1$, where the *Fresnel number* (a) $N_F = 2$, (b) $N_F = 5$, (c) $N_F = 10$, and (d) $N_F = 20$. Inspection will show that the diffraction patterns have essentially N_F large-scale ripples across the aperture width. Compare the intensity patterns obtained above with that observed at the slit plane $\zeta = 0$.
3. Repeat 2 by evaluating the DFT of $\tilde{U}(q_\xi, 0) \exp(-i\zeta q_\xi^2/4)$ in Eq. (1.4.6). Use $N = 2^5$ points, and analyze the accuracy of these results.
Hint: use a sampling rate $\Delta q_\xi = \pi$ in order to obtain a DFT in the range $|\xi| \leq 1$.

4. Show that the Fraunhofer diffraction pattern of a slit can be set as:

$$\tilde{u}_F(\xi, \zeta) = \frac{\exp(i\xi^2/\zeta)}{\sqrt{i\pi\zeta}} \operatorname{sinc}(\xi/\zeta), \quad \zeta \gg 1. \quad (1.4.11)$$

Hint: use Eq. (1.4.7) with $\tilde{f}_\zeta(\xi) = \operatorname{rect}(\xi)$. Alternatively you may use the asymptotic expansion $\operatorname{erf}(t) = (2t/\sqrt{\pi}) \exp(-t^2)$, as $t \rightarrow 0$, in Eq. (1.4.10).

5. Plot the normalized intensity patterns $|\tilde{u}(\xi, \zeta)|^2$, given in Eq. (1.4.10), at planes $\zeta = 1/(4\pi N_F)$ within the range $|\xi| \leq \max(1, 2\pi\zeta)$, where (a) $N_F = 1/20$, (b) $N_F = 1/10$, (c) $N_F = 1/5$, and (d) $N_F = 1/2$. Compare the intensity patterns evaluated above with $|\tilde{u}_F(\xi, \zeta)|^2$ obtained in the far field (1.4.11).

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