

1 **Comparison of simultaneous saccharification and fermentation**  
2 **and separate hydrolysis and fermentation processes for butanol**  
3 **production from rice straw**

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22 **Abstract**

23 Rice straw (RS) is one of the lignocellulosic wastes with the highest global production. The  
24 main objective of this study was to maximise the butanol production by *Clostridium beijerinckii*  
25 DSM 6422 from RS pretreated by microwave-assisted hydrothermolysis. Two different  
26 fermentation strategies were compared: separate hydrolysis and fermentation (SHF, two-step  
27 process) and simultaneous saccharification and fermentation (SSF, one-step process). In  
28 parallel, the variables that significantly affected the butanol production were screened by using  
29 fractional factorial designs. Butanol concentration and productivity at 48 h were, respectively,  
30 8% and 173% higher in SSF than in SHF. A one-step process was more efficient than a two-  
31 step process, especially considering the time savings derived from much higher productivity.  
32 From these results, SSF was further optimised by response surface methodology with central  
33 composite design over the key factors on the butanol production at 48 h: initial pH, enzyme  
34 loading and yeast extract concentration. The optimum point yielded a butanol productivity of  
35  $0.114 \text{ g L}^{-1} \text{ h}^{-1}$ , with a butanol-biomass ratio of  $51 \text{ g kg}^{-1}$  of raw RS (ABE-biomass ratio of  $77.0$   
36  $\text{g kg}^{-1}$  of raw RS). The parameter with the greatest effect was enzyme loading, with an optimal  
37 value of  $13.5 \text{ FPU g-dw}^{-1}$ . This study showed that microwave-processed RS has great potential  
38 as a substrate for the butanol production from ABE fermentation when combining process  
39 stages by SSF.

40

41 **Keywords:** Butanol, lignocellulosic waste, microwave thermohydrolysis, rice straw,  
42 simultaneous saccharification/fermentation

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## 44 1 Introduction

45 The expected increase of the world population by more than 30% in the next 40 years, the  
46 depletion of resources, external energy dependence and climate change are altering the way in  
47 which biological resources in Europe are managed. In this context, interest in biomass as a  
48 source of carbon and energy has increased [1]. Lignocellulosic material is the most abundant  
49 and economical biomass on the planet [2]. Numerous raw materials, such as agricultural  
50 residues, forestry wastes, industrial and municipal wastes, and bioenergy crops, are available  
51 for the production of biofuels, including biobutanol [3]. However, a pretreatment is necessary  
52 to alter the lignocellulosic structure and to remove and/or alter lignin, generally followed by an  
53 enzymatic or acid hydrolysis stage to obtain sugar monomers [4].

54 Biobutanol is mainly produced by *Clostridium acetobutylicum* or *C. beijerinckii* in  
55 acetone-butanol-ethanol (ABE) fermentation by a pathway consisting of two metabolic phases:  
56 acidogenesis, followed by solventogenesis [5]. During acidogenesis bacterial growth occurs  
57 with the production of acids, hydrogen and carbon dioxide; whereas in the solventogenesis stage  
58 the production of solvents and endospore formation occurs [6]. These gram-positive and  
59 anaerobic bacteria belong to the only genus capable of producing this solvent as a major  
60 metabolite [7]. Butanol has some benefits as a fuel in terms of energy density, handling,  
61 transport and storage [8]. Despite these advantages, its production by fermentation cannot  
62 compete economically with the butanol obtained in the petrochemical industry due to, among  
63 other causes, lower development of bioprocesses, long fermentation times, high cost of the  
64 substrate, low yields and high cost of product recovery [9]. Strategies developed to enhance  
65 cellulosic biobutanol production include strain improvement by genetic engineering,  
66 optimisation of the medium formulation and combination of ABE fermentation stages [4]. To  
67 screen and optimise the effect of medium conditions and process parameters on ABE

68 productivity, statistical techniques such as fractional factorial design and response surface  
69 methodology (RSM) are often used [10].

70 The processes derived from the combination of ABE fermentation stages are  
71 simultaneous saccharification and fermentation (SSF), consolidated bioprocessing (CBP),  
72 separate hydrolysis and fermentation with *in-situ* recovery (SHFR) and simultaneous  
73 saccharification and fermentation with *in-situ* recovery (SSFR) [4]. SSF was developed by  
74 Gauss et al. [11] and combines enzymatic hydrolysis and ABE fermentation in one step,  
75 increasing the butanol yield and productivity compared to separate hydrolysis and fermentation  
76 (SHF). SSF could potentially reduce operational costs and the risk of contamination. In  
77 addition, the SSF process minimises glucose inhibition on cellulases and  $\beta$ -glucosidase because  
78 bacteria consume sugars as soon as they are released [4]. For example, Qi et al. [12] observed  
79 that butanol production was higher in SSF (12.64 g L<sup>-1</sup>) than in SHF (11.25 g L<sup>-1</sup>) by fermenting  
80 ammonium sulfite-pretreated wheat straw with *C. acetobutylicum* ATCC 824, despite  
81 decreasing the biomass loading from 10.5 to 9% (w/v). Not only was SSF more efficient in  
82 terms of butanol production and time, but enzyme loading was reduced by one-half, thereby  
83 conferring an economic advantage. However, Shao and Chen [13] obtained a shorter  
84 fermentation time and a higher butanol concentration by the same bacterial strain from  
85 *Amorphophallus* konjac waste in SHF, suggesting that the most appropriate process depends  
86 on factors such as the feedstock type and the strain of bacteria used.

87 One of the most abundant lignocellulosic wastes in the world is rice straw (RS), with an  
88 estimated annual production of 731 million tons [14]. Unlike other straws, RS is not generally  
89 used as animal feed due to its low digestibility and, apparently, it has a low value for social  
90 benefit, so it is burnt openly in the field, causing air pollution [15]. There are numerous reported  
91 pretreatments (physical, chemical, physicochemical and biological) to enhance ABE  
92 fermentation of RS [16]. Despite the low lignin content in RS [17], these methods must face

93 other limiting factors, such as the presence of accumulated silica [18] and high cellulose  
94 crystallinity [19]. Among these pretreatment options, dielectric heating by microwave  
95 irradiation is used on lignocellulose as an alternative to convection heating [20]. Indeed, Ma et  
96 al. [21] noticed that microwave pretreatment could improve the enzymatic accessibility of  
97 cellulose by partially breaking the lignin-hemicellulose structure and the waxy structure of  
98 silicon, increasing solubility. Furthermore, Zhu et al. [19] determined that, compared to the  
99 alkali-alone process, microwave-assisted alkali pretreatment eliminates more hemicellulose and  
100 lignin from RS, consequently obtaining a hydrolysate with more glucose and less xylose after  
101 enzymatic hydrolysis. One of the limitations for the production of biobutanol is the generation  
102 during pretreatment of compounds that inhibit microbial growth, such as acetic acid, 5-  
103 hydroxymethylfurfural (HMF) and furfural [16]. After pretreating RS with dilute acid, Hsu et  
104 al. [17] observed a correlation between the generation of these compounds and pretreatment  
105 severity. Indeed, Fonseca et al. [22] demonstrated that detoxification of rice improved the  
106 ethanol productivity from RS hydrolysate with dilute acid. Another alternative to overcome  
107 the toxicity derived from chemical pretreatment is the use of non-catalysed methods such as  
108 microwave irradiation. This strategy can avoid problems of inhibition by these compounds,  
109 saving at the same time the cost derived from chemicals. Although SSF processes have been  
110 reported for butanol production by ABE fermentation using other agricultural waste such as  
111 wheat straw [8,12,23], corn stover [24] or corncob [25], among others, there is no literature data  
112 on the effect of using SSF to produce butanol from RS.

113 The scope of this work is to evaluate the SSF process for butanol production by *C.*  
114 *beijerinckii* DSM 6422 from RS previously treated by microwave-assisted hydrothermolysis.  
115 SSF configuration was compared with SHF in terms of butanol productivity by evaluating the  
116 effect of the following parameters: type of buffer (citrate or acetate) and enzyme loading for  
117 enzymatic hydrolysis; and initial pH, yeast extract concentration and iron concentration in the

118 fermentation broth in two sets of fractional factorial design experiments. In a later stage, SSF  
119 was further optimised using RSM with central composite design (CCD) over variables with  
120 statistically significant effects.

## 121 **2 Materials and methods**

### 122 2.1 Materials

123 RS was obtained from local farmers of L'Albufera located near Valencia (Spain). The  
124 biomass was dried for 24 h at room temperature, cut into fragments of ~2 cm and milled. Particle  
125 size between 100 and 500  $\mu\text{m}$  was selected by ISO-3310.1 sieve (CISA, Spain), afterwards it  
126 was dried in an oven at 45 °C until the residual moisture content was less than 5% (w/w), and  
127 it was then stored for further use. The commercial enzyme blend Cellic<sup>®</sup> CTec2 (Novozyme,  
128 Denmark) was employed for hydrolysis of the pretreated RS. The cellulase activity of the  
129 enzyme was measured according to the method of the National Renewable Energy Laboratory  
130 (NREL) [26], resulting in a value of 119 filter paper units (FPU)  $\text{mL}^{-1}$ .

### 131 2.2 RS pretreatment

132 Microwave-assisted hydrothermal hydrolysis was performed in an ETHOS One  
133 microwave digestion system (Milestone, Italy). The microwave had a maximum power of 1500  
134 W and was controlled via a microprocessor with a capacity of 10 TFM vessels (an internal  
135 temperature sensor was installed in a reference vessel). The RS was pretreated at 10% (w/v)  
136 using 3 g of dry biomass in 30 mL of deionized water. The microwave was heated using the  
137 following ramp of temperature: an initial increase to 100 °C at a rate of 15 °C  $\text{min}^{-1}$ , which was  
138 then increased at 6 °C  $\text{min}^{-1}$  until 160 °C and then to 4 °C  $\text{min}^{-1}$  until 200 °C, holding at 15 min  
139 [27]. Once the heating was finished, the vessels were cooled at room temperature. The slurry  
140 was centrifuged at 10000 rpm for 5 min (centrifuge 5804, Eppendorf, Germany), and the solid

141 phase was washed with deionized water and pH was adjusted to 6.5. Finally, the pretreated RS  
142 was dried at 45 °C.

### 143 2.3 Microorganism and inoculum preparation

144 The bacterial strain *Clostridium beijerinckii* DSM 6422 (NRRL B-592) was supplied by  
145 the Leibniz Institute DSMZ-German Collection of Microorganisms and Cell Cultures  
146 (Braunschweig, Germany). The strain was stored at -80 °C in a Reinforced Clostridial Medium  
147 (RCM) with 20% (v/v) glycerol. Before fermentation, the cells were grown in 50-mL serum  
148 bottles containing 40 mL of modified RCM (19 g L<sup>-1</sup> RCM supplemented with 10 g L<sup>-1</sup> glucose)  
149 under anaerobic conditions by sparging pure nitrogen in the medium. The inoculum was  
150 statically incubated at 37 °C for 24 h. The media used in the cryopreservation and the inoculum  
151 preparation were sterilized in an autoclave for 21 min at 121 °C.

### 152 2.4 ABE fermentation

#### 153 2.4.1 ABE fermentation by SHF

154 Pretreated RS was hydrolysed prior to fermentation in a separate vessel using the  
155 commercial enzyme blend Cellic<sup>®</sup> CTec2. Enzymatic hydrolysis was carried out in a 100-mL  
156 conical flask (with 50 mL of working volume) in a SI500 orbital shaker (Stuart, UK). The  
157 hydrolysis process was performed at 50 °C and 150 rpm for 72 h with a biomass loading of 10%  
158 (w/v) and an enzyme dosing of 4.1 FPU g-dw<sup>-1</sup>. The buffer employed was citrate (50 mM) or  
159 acetate (50 mM), whose effects on ABE fermentation were assessed using the fractional  
160 factorial design of the experiment described in section 2.6. The initial pH was adjusted to 5.0  
161 by NaOH and HCl. After enzymatic hydrolysis, the samples were centrifuged (6 min, 4000  
162 rpm), filtered by 1.2 µm and stored at 4 °C for a maximum of 12 h before fermentation. A  
163 volume of 34.6 mL of the enzymatic hydrolysate was fermented in 50-mL serum bottles with a  
164 working volume of 40 mL. The concentration of the buffer and the minerals was based on a

165 modified P2 medium introduced by Monot et al. [28]: 0.50 g L<sup>-1</sup> KH<sub>2</sub>PO<sub>4</sub>, 0.50 g L<sup>-1</sup> K<sub>2</sub>HPO<sub>4</sub>,  
166 2.20 g L<sup>-1</sup> NH<sub>4</sub>OAc, 0.09 g L<sup>-1</sup> MgSO<sub>4</sub>·7H<sub>2</sub>O and 0.001 g L<sup>-1</sup> MnSO<sub>4</sub>·H<sub>2</sub>O. The resazurin  
167 concentration was set to 1 mg L<sup>-1</sup>. FeSO<sub>4</sub>·7H<sub>2</sub>O and yeast extract were added in concentrations  
168 of 0.01 or 0.02 g L<sup>-1</sup> and 2 or 4 g L<sup>-1</sup> respectively, and the initial fermentation pH was adjusted  
169 to 6.4 or 7.4, according to the fractional factorial design of the experiment. Beforehand, the  
170 sealed bottles were autoclaved for 10 min at 121 °C; the oxygen was displaced by sparging pure  
171 nitrogen. The inoculation was carried out with 2 mL (5% v/v) of actively growing cells, and the  
172 serum bottles were incubated at 37 °C and 150 rpm for 72 h.

#### 173 2.4.2 ABE fermentation by SSF

174 In this configuration, the pretreated RS was simultaneously hydrolysed and fermented  
175 in a 50-mL serum bottle (working volume of 40 mL) with a biomass loading of 9% (w/v). The  
176 medium for conducting the SSF experiments was the same as that for the SHF experiments,  
177 except that no hydrolysis buffer (50 mM citrate or acetate) was added as the fermentation media  
178 contained 28.5 mM of acetate. The effect of the same media parameters (iron and yeast extract  
179 concentrations) as in SHF was assessed by the fractional factorial design of the experiment. In  
180 this case, the initial reaction pH was set to 5.2 or 6.2 as representatives of optimum values for  
181 saccharification or fermentation respectively. The oxygen was displaced by sparging pure  
182 nitrogen before autoclaving for 10 min at 121 °C. Afterwards, the enzyme was added along with  
183 the inoculum. A loading of 4.1 or 12.4 FPU g-dw<sup>-1</sup> of Cellic<sup>®</sup> CTec2 was used in the fractional  
184 factorial design experiments in order to assess its influence in SSF. The inoculation was carried  
185 out with 2 mL (5% v/v) of actively growing cells. The SSF bottles were incubated at 37 °C and  
186 150 rpm for 120 h. Additionally, two independent replicates of a control experiment (without  
187 inoculation) were carried out with the maximum enzyme loading (12.4 FPU g-dw<sup>-1</sup>) at the  
188 minimum pH (5.2) in order to evaluate the maximum release of monosaccharides from the



189 pretreated RS. From results obtained as described herein, CCD was used for further  
190 optimisation of the SSF results.

## 191 2.5 Analytical methods

192 The structural carbohydrates, lignin and the moisture content of the RS were determined  
193 according to the National Renewable Energy Laboratory (NREL) procedures [29]. The  
194 characterisation of the fermentation was carried out by the analysis of pH, cell growth,  
195 production of acids and solvents, and sugar uptake from 1-mL samples collected at appropriate  
196 times. The pH was measured by a Minitrode electrode (Hamilton, USA). Cell density ( $\text{g-dw L}^{-1}$ )  
197 <sup>1</sup>) was calculated from the optical density at 600 nm ( $\text{OD}_{600}$ ) measured in a spectrophotometer  
198 (SpectroFlex 6600, WTW, Germany). The correlation between  $\text{OD}_{600}$  and cell density was  
199 determined as follows:  $\text{g-dw L}^{-1} = 0.2153 \cdot \text{OD}_{600} + 0.0689$  ( $n = 10$ ,  $R^2 = 0.9907$ ). Samples were  
200 centrifuged at 10000 rpm for 5 min, and the supernatant was filtered by 0.22  $\mu\text{m}$  before  
201 chromatographic analysis. Acids (acetic acid and butyric acid) and solvents (butanol, acetone  
202 and ethanol) were analysed in a gas chromatograph (TRACE GC Ultra, Thermo Scientific,  
203 USA) equipped with a Teknokroma TRB-FFAP capillary column ( $30 \text{ m} \times 0.25 \text{ mm} \times 0.25 \mu\text{m}$ ),  
204 with helium as carrier gas at a flow rate of  $1 \text{ mL min}^{-1}$ . One microliter of acidified samples was  
205 injected at  $250 \text{ }^\circ\text{C}$  (10:1 split ratio), and the compounds were detected in a flame ionization  
206 detector at  $250 \text{ }^\circ\text{C}$ . The oven temperature was held at  $50 \text{ }^\circ\text{C}$  for 4 min, increased at  $30 \text{ }^\circ\text{C min}^{-1}$   
207 until  $80 \text{ }^\circ\text{C}$  (hold time 3 min), and increased at  $20 \text{ }^\circ\text{C min}^{-1}$  until  $210 \text{ }^\circ\text{C}$  (hold time 5 min).  
208 Sugars (glucose, xylose and arabinose) were analysed by an ion chromatograph (883 Basic IC  
209 plus, Metrohm, Switzerland) equipped with an amperometric detector and a Metrosep Carb 2  
210 anion exchanger column ( $150 \text{ mm} \times 4 \text{ mm} \times 5 \mu\text{m}$ ). The mobile phase (20 mM NaOH) was set  
211 at a flow rate of  $0.5 \text{ mL min}^{-1}$ . Data are the mean of, at least, two technical replicates.

212 For the evaluation of the process performance, the following parameters were used:

213 
$$\text{Butanol (or ABE) – biomass ratio (g kg}^{-1}\text{)} = \frac{\text{Butanol (or ABE) produced (g)}/V_{\text{hydrolysate fermented (L)}}}{[\text{Biomass loading (kg L}^{-1}\text{)}/\text{Solid recovery (\%)}]\times 100} \quad (1)$$

214 
$$\text{Butanol (or ABE) productivity (g L}^{-1}\text{ h}^{-1}\text{)} = \frac{\text{Butanol (or ABE) concentration (g L}^{-1}\text{)}}{\text{Total reaction time (h)}} \quad (2)$$

215 
$$\text{Butanol (or ABE) yield (g g}^{-1}\text{)} = \frac{\text{Butanol (or ABE) concentration (g L}^{-1}\text{)}}{\text{Sugar consumed (g L}^{-1}\text{)}} \quad (3)$$

216 To compare the reaction time of the SHF process with that of SSF, the total reaction  
 217 time of hydrolysis plus fermentation was assessed. Solid recovery refers to biomass recovered  
 218 after pretreatment expressed as a percentage.

## 219 2.6 Design of experiments and statistical analysis

220 In this work, SSF was first assessed and compared with SHF, by fractional factorial  
 221 designs. As the SSF process performed better than the SHF process, the significant variables  
 222 for SSF were further optimised by RSM using CCD. The response variable in all cases was the  
 223 concentration of butanol produced at 48 h. The commercial software MINITAB<sup>®</sup> v.18.1 (LEAD  
 224 Technologies, Inc.) was used for the design of experiments, regression analysis and analysis of  
 225 variance (ANOVA) at a confidence level of 95% (p-value < 0.05).

### 226 2.6.1 Fractional factorial design and data analysis

227 A 2<sup>4+1</sup> fractional factorial design (resolution IV, 8 experiment runs) was used to identify  
 228 the significant factors affecting butanol production at 48 h both in SHF and SSF processes. The  
 229 effects of three variables (low level and high level) – yeast extract concentration (2 and 4 g L<sup>-1</sup>)  
 230 <sup>1</sup>), FeSO<sub>4</sub>·7H<sub>2</sub>O concentration (0.01 and 0.02 g L<sup>-1</sup>) and initial fermentation pH (6.4 and 7.4 for  
 231 SHF, and 5.2 and 6.2 for SSF, respectively) – were evaluated in both processes. For SHF, the  
 232 fourth variable was the buffer employed for enzymatic hydrolysis (50 mM acetate and 50 mM  
 233 citrate), whereas for SSF it was the enzyme loading (4.1 and 12.4 FPU g-dw<sup>-1</sup>).

### 234 2.6.2 Central composite design and data analysis

235 After identification of significant factors, an RSM with CCD was used in the SSF  
236 process to determine the optimal combination of enzyme loading, initial pH and yeast extract  
237 concentration for maximising butanol production. The established range for each factor was as  
238 follows: enzyme loading (from 5.4 to 19.1 FPU g-dw<sup>-1</sup>), initial pH (from 5.6 to 7.2) and yeast  
239 extract concentration (from 0.5 to 5.5 g L<sup>-1</sup>). Table 1 summarises the coded and real values of  
240 the three variables used in CCD, which comprised a total of 20 experimental runs with 6 central  
241 point replications. Finally, a validation step was carried out by three replicates using the  
242 optimised conditions for butanol production.

### 243 3 Results and discussion

#### 244 3.1 Pretreatment of RS

245 Microwave-assisted hydrothermolysis was selected as RS pretreatment since it presents  
246 short reaction times, uniform and rapid heating of biomass, lower generation of inhibitory  
247 compounds, higher removal of acetyl groups in hemicellulose, and lower costs in comparison  
248 with acid or alkaline pretreatments [30]. The chemical compositions of the raw and pretreated  
249 RS are presented in Figure 1. The untreated dried material consisted of 35.8 ± 2.1% glucan,  
250 14.8 ± 1.6% xylan, 2.7 ± 0.4% arabinan, 0.1 ± 0.0% acid soluble lignin, 14.3 ± 0.4% acid  
251 insoluble lignin and 16.7 ± 0.1% ash. This composition is in the typical value range found for  
252 RS of different sources [31,32]. Recently, Passoth and Sandgren [33] reported that the typical  
253 values for the three major polymers ranged from 29.2 to 34.7% for cellulose, 12.0 to 29.3% for  
254 hemicellulose, and 17.0 to 19.0% for lignin, being silica the major ash component.

255 The pretreatment resulted in a solid recovery of 80.5% of the raw RS with different  
256 degrees of degradation among carbohydrate fractions. For example, the glucan percentage  
257 increased from 35.8 to 39.4%, although the total percentage of carbohydrates remained almost  
258 stable at ~53% due to the loss of hemicellulose. During pretreatment only 11.5% of glucan was

259 lost, but greater degradation of arabinan and xylan was observed, with losses of 50.6% and  
260 34.5% respectively. These results indicated that some hemicellulose was removed in the  
261 microwave pretreatment of RS; phenomena also observed by Zhu et al. [19] at lower irradiation  
262 powers. Higher values of polysaccharides were recovered from raw RS (80.1%) when  
263 compared to previous studies on this type of biomass. For example, Amiri et al. [34] obtained  
264 a recovery of 76.2% after organosolv pretreatment with a 75% (v/v) ethanol and 1% (w/w)  
265 sulfuric acid solution at 150 °C during 30 min, and Moradi et al. [35] found a value of 51.9%  
266 after 3 h of alkaline pretreatment at 0 °C with a 12% (w/v) NaOH solution. The microwave  
267 irradiation at the tested conditions resulted in a 13.3% delignification and removed 13.7% of  
268 ashes (silica content), thus improving the RS digestibility. However, the delignification degree  
269 obtained in this study could impact the saccharification of the waste, since lignin binds non-  
270 productively to cellulase due to its hydrophobic nature [36]. On the other hand, the remaining  
271 silica in the pretreated RS could also act as a physical barrier, protecting for enzymatic  
272 hydrolysis [37].

### 273 3.2 Comparison of ABE fermentation by SHF and SSF: screening of key factors

274 The  $2^{4-1}$  fractional factorial design was conducted for the SHF and SSF processes to  
275 evaluate the influence of the selected parameters on butanol production. The experimental  
276 design and the response results for both processes are shown in Table 2. The analysis of  
277 variance (ANOVA) of the outcomes, with the estimated coefficients and significant levels for  
278 the regression model and the evaluated variables for the SHF and SSF processes are shown in  
279 supplementary material. In both cases, after 72 h of fermentation the concentrations of butanol  
280 and ABE increased less than 1% from 48 h. Therefore, butanol production at 48 h was  
281 considered as the response variable. The fast rate of solvent production demonstrated the  
282 successful balance between the acidogenic and solventogenic metabolic phases of *Clostridium*  
283 *beijerinckii* DSM 6422 using both the appropriate operational conditions and the adequate

284 biomass pretreatment. Models for SHF and SSF were statistically significant, with p-values  
285 lower than 0.05. In addition, the values of the coefficient of determination ( $R^2$ : 0.9996 and  
286 0.9997 for SHF and SSF, respectively) and the adjusted coefficient of determination (Adj.  $R^2$ :  
287 0.9975 and 0.9976 for SHF and SSF, respectively) were close to 1.0, indicating the goodness of  
288 fit of the models.

289 From the two-step process (SHF) results, among the four variables screened, only the  
290 type of buffer used during enzymatic hydrolysis was found to be significant (p-value of 0.0120).  
291 The linear coefficient of the buffer factor (low-high level: acetate-citrate) was lower than zero,  
292 indicating that the use of citrate buffer during the saccharification step negatively affected  
293 butanol production. Citrate buffer at 50 mM is widely used to maintain a pH around 5.0 during  
294 enzymatic hydrolysis [34,35,38]. Furthermore, Xue et al. [39] showed that 60 mM citrate buffer  
295 was optimum for ABE fermentation of Jerusalem artichoke stalk with *C. beijerinckii* CC101,  
296 lower and higher values decreased solvent production. Contrarily, Liu et al. [40] observed that  
297 *C. beijerinckii* NCIMB 8052 did not grow with 50 mM citrate; whereas when acetate was used  
298 as a buffer ABE fermentation was not inhibited. In our study, butanol concentrations ranged  
299 from 2.72 to 3.16 g L<sup>-1</sup> by using citrate buffer, while a minimum of 4.68 g L<sup>-1</sup> was obtained in  
300 the experiments with acetate as hydrolysis buffer. Our results corroborated that the use of citrate  
301 buffer provokes a negative effect on ABE fermentation of pretreated RS by *C. beijerinckii* DSM  
302 6422. The yeast extract concentration did not show a significant effect in the tested range of 2  
303 to 4 g L<sup>-1</sup>. Contrarily, a significant impact on the production of butanol by *C. acetobutylicum*  
304 MTCC 481 from RS hydrolysate was previously observed, with an optimal concentration of 3  
305 g L<sup>-1</sup> [41]. Thus, this demonstrates the importance of the preliminary screening of the media  
306 composition for each specific lignocellulosic waste and bacterial strain. The non-significant  
307 effect of iron on butanol production from RS hydrolysate indicates that the quantity containing  
308 the raw material along with the amount from the minimum yeast extract concentration supplied

309 to the fermentation broth is sufficient. Gottumukkala et al. [38] determined that the  
310 improvement in solvent production by *C. sporogenes* BE01 after removing mineral  
311 supplementation from RS hydrolysate could be due to the presence of these minerals in the raw  
312 material. Ranjan et al. [41] also found that iron concentration had no impact on ABE  
313 fermentation of RS with *C. acetobutylicum* MTCC 481 supplemented with 3 g L<sup>-1</sup> of yeast  
314 extract. Furthermore, the initial fermentation pH was incorporated into the experimental design  
315 since it would affect the biochemical and biophysical characteristics of the solventogenic  
316 *Clostridium* spp. [42]. Fermentation pH, together with the rate of acid production, is one  
317 potential key factor in the concentration of undissociated acids that can inhibit a correct shift  
318 towards solventogenesis [43]. In contrast, fermentation pH was found to be non-significant,  
319 likely because the sugar concentration released from enzymatic hydrolysis was not sufficiently  
320 high enough to unbalance the rate of acid production.

321 In the case of the one-step process (SSF), two variables were found to be statistically  
322 significant. The initial pH had a great effect on butanol production (p-value of 0.0164).  
323 Furthermore, the enzyme loading was also significant (p-value of 0.0277). Based on the coded  
324 coefficients of the linear effects, the order of importance was as follows: initial pH (1.2041) >  
325 enzyme loading (0.7130). These results show that, for SSF, it is better not to use a value near  
326 to the optimum for the saccharification of cellulosic materials as the initial pH. Although  
327 enzymatic hydrolysis will proceed slowly, solventogenic shift would be favoured. Even though  
328 no interaction between initial fermentation pH and enzyme loading had a significant effect, the  
329 need to use a pH above the optimum for enzymatic hydrolysis could explain the higher enzyme  
330 loading required in SSF (12.4 FPU g-dw<sup>-1</sup>) to achieve butanol concentrations above 4 g L<sup>-1</sup>  
331 compared with the SHF process (4.1 FPU g-dw<sup>-1</sup>). Furthermore, the in-situ ABE products in  
332 SSF can be linked to the higher enzyme requirements, as they have been shown as inhibitors of  
333 the cellulolytic and hemicellulolytic enzyme activity [44]. Contrarily, the fermentation

334 temperature selected (37 °C) has been reported as a more suitable temperature in comparison to  
335 50 °C for better cellulase and xylanase activities in the presence of ABE products [44].

336 Both configurations were compared in terms of process efficiency. Table 3 summarises  
337 the experimental data obtained in the runs with the highest butanol production at 48 h for each  
338 configuration (run 7-SHF, run 8-SSF). The values of released sugars ( $\text{g L}^{-1}$ ), butanol and ABE  
339 production ( $\text{g L}^{-1}$ ), butanol and ABE yield ( $\text{g g}^{-1}$ ), butanol and ABE-biomass ratio ( $\text{g kg RS}^{-1}$ ),  
340 and butanol and ABE productivity ( $\text{g L}^{-1} \text{h}^{-1}$ ) are included. After 72 h of enzymatic hydrolysis  
341 (SHF), the concentrations obtained of glucose, xylose and arabinose were 17.68, 6.10 and 0.39  
342  $\text{g L}^{-1}$  respectively. In order to evaluate the maximum sugars released in the SSF processes, two  
343 control saccharification assays without inoculum (initial pH = 5.2, enzyme loading = 12.4 FPU  
344  $\text{g-dw}^{-1}$ ) were carried out, with average glucose, xylose and arabinose concentrations of 18.92,  
345 6.91 and 0.64  $\text{g L}^{-1}$  respectively. Regardless of the process used, the concentrations of sugars  
346 released by the enzyme blend Cellic<sup>®</sup> CTec2 from the pretreated RS were very similar (~50%  
347 sugar recovery). Thus, corroborating the idea that the need for higher enzyme dosing in SSF  
348 than in SHF relies on the enzymatic inhibition by ABE products and/or on the impossibility of  
349 performing the saccharification at the optimum pH. The delignification (13.3%) combined with  
350 the ash removal (13.7%) achieved after microwave pretreatment limited, to some extent, the  
351 sugar recovery from enzymatic hydrolysis. Concerning the SHF configuration, the butanol  
352 concentration at 48 h was 4.85  $\text{g L}^{-1}$  with an ABE concentration of 7.95  $\text{g L}^{-1}$  (butanol:acetone  
353 mass ratio of 1.6:1, ethanol was not detected). All the released sugars were consumed at the end  
354 of the fermentation, resulting in a butanol (ABE) yield of 0.245  $\text{g g}^{-1}$  (0.402  $\text{g g}^{-1}$ ). The RS  
355 exploitation was evaluated with the butanol or ABE-biomass ratio, with observed values of 44.6  
356  $\text{g}$  of butanol and 73.1  $\text{g}$  of ABE per  $\text{kg}$  of raw RS. In the SSF process, the butanol concentration  
357 at 48 h of reaction time (5.24  $\text{g L}^{-1}$ ) increased by 8% of that observed in SHF and, in turn, the  
358 butanol-biomass ratio rose to 48.2  $\text{g kg RS}^{-1}$ ; whereas the ABE concentration (butanol:acetone

359 mass ratio of 1.8:1, ethanol was not detected) increased only by 3.7%. The total concentration  
360 of sugars in the fermentation broth was  $< 1.5 \text{ g L}^{-1}$  and the butanol (ABE) yield resulted in  
361  $0.217 \text{ g g}^{-1}$  ( $0.341 \text{ g g}^{-1}$ ) considering the maximum sugar concentration released in the two  
362 control experiments. It should be noted that both glucose and xylose were nearly completely  
363 consumed by the microorganisms, thus, maximum utilisation of the sugars released in the  
364 saccharification step was reached. Guan et al. [45] also pointed out that the SHF process showed  
365 higher ABE yields than those obtained in the SSF process from fermenting Kraft paper mill  
366 sludge by *C. acetobutylicum* ATCC 824.

367         The most remarkable difference between the one-step and two-step processes was found  
368 in the overall butanol productivity. A productivity of  $0.040 \text{ g L}^{-1} \text{ h}^{-1}$  was achieved in the SHF  
369 process, while a value 2.7-fold higher ( $0.109 \text{ g L}^{-1} \text{ h}^{-1}$ ) was reached in the SSF process. This  
370 greater productivity is related not so much to the increase (by 8%) in the final butanol  
371 concentration but instead to the lower operation time needed to carry out the valorisation  
372 process of the RS. The SHF process needed a total of 120 h (72 h of enzymatic hydrolysis  
373 followed by 48 h of fermentation), while in the SSF process only 48 h were required to complete  
374 the butanol production at the same or even slightly higher levels than in the two-step process.  
375 Furthermore, the SSF process showed greater exploitation of the RS with a higher butanol-  
376 biomass ratio. Other authors compared the simultaneous process to the conventional SHF in the  
377 production of butanol from wheat straw [8,12], showing that SSF was more efficient and time-  
378 saving than SHF. Our results corroborated previous findings, revealing the potential of SSF to  
379 be less expensive than SHF in butanol production from the hydrolysate of straw. The greater  
380 efficiency of the SSF process could imply a reduction in equipment investment (only one vessel  
381 is necessary) and operational costs (lower production times, less contamination risk) in the  
382 production of butanol from RS.

383 3.3 Optimization of butanol production by SSF



384 Based on the above results, a RSM with full factorial CCD was performed for the SSF  
385 process to maximise butanol production by optimising three factors: enzyme loading, initial pH  
386 and yeast extract concentration. The model was validated by performing an experiment, with 3  
387 replicates, at the optimum conditions.

### 388 3.3.1 Response surface methodology

389 The response surface methodology approach consisted of a five-level, three-factor CCD  
390 (Table 1) and subsequent linear regression analysis to fit the experimental data with a second-  
391 order model. Three independent variables were selected for the determination of the main  
392 effects and their interactions on butanol production. Enzyme loading ( $Z_1$ ) and initial pH ( $Z_2$ ),  
393 were found to be significant in the fractional factorial design of the SSF process, whereas yeast  
394 extract concentration ( $Z_3$ ) was included for further study by enlarging its variation range. Based  
395 on the previous results,  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$  concentration was set to  $0.02 \text{ g L}^{-1}$ . Table 4 shows the  
396 CCD experimental matrix with variables in real terms and the observed and predicted values of  
397 butanol concentration after 48 h obtained from each condition. A total of 20 experimental runs  
398 were carried out, including 6 central point replications to check the experimental variability.  
399 The experimental results showed that the one-step process succeeded in producing butanol after  
400 48 h within the ranges of the independent variables, achieving butanol concentrations from 1.06  
401 to  $5.31 \text{ g L}^{-1}$ . Data of run 15 was not included due to oxygen contamination detected by a  
402 resazurin indicator. The greater butanol production ( $5.31 \text{ g L}^{-1}$ ) was obtained in run 14 with an  
403 ABE concentration of  $8.48 \text{ g L}^{-1}$  and a butanol:acetone mass ratio of 1.7:1 (ethanol was not  
404 detected). Furthermore, a butanol productivity of  $0.111 \text{ g L}^{-1} \text{ h}^{-1}$  was reached with a butanol  
405 yield of  $0.298 \text{ g g}$  of consumed sugar<sup>-1</sup> and a butanol-biomass ratio of 48.8 g per kg of raw RS  
406 (ABE-biomass ratio of 78.0 g per kg of raw RS). The second-order model obtained for the  
407 concentration of butanol ( $\text{g L}^{-1}$ ) in terms of actual factors was as follows:

*Butanol concentration* (4)

$$\begin{aligned} &= -41.9 + 1.018Z_1 + 10.69Z_2 + 3.26Z_3 - 0.0641Z_1^2 - 0.804Z_2^2 - 0.1304Z_3^2 \\ &+ 0.0783Z_1Z_2 + 0.0039Z_1Z_3 - 0.324Z_2Z_3 \end{aligned}$$

408

409         The analysis of variance (ANOVA) and coded regression coefficients of the second-  
410 order model for butanol production are presented in Table 5. The model was highly significant  
411 at the 95% significance level, with a p-value of 0.0015, whereas the lack-of-fit was not  
412 significant (p-value of 0.0500). The low standard deviation (SD) value of 0.5037 g L<sup>-1</sup>,  
413 measured in the units of the response variable indicates that the data values are not far from the  
414 fitted values. The coefficient of determination (R<sup>2</sup>) value was 0.9004, showing a good  
415 correlation between the experimental results and the predicted values, in which only 9.96% of  
416 the total variations were not explained by the model. The goodness of the predictions was also  
417 confirmed by the adjusted coefficient of determination (Adj. R<sup>2</sup>: 0.8008), suggesting that this  
418 model could properly predict the effect of enzyme loading, initial pH and yeast extract on  
419 butanol production after 48 h from RS by SSF. As can be seen from the ANOVA of the model,  
420 only the linear coefficients of enzyme loading (Z<sub>1</sub>) and yeast extract concentration (Z<sub>3</sub>) were  
421 found to be significant (p-value of 0.0037 and 0.0009, respectively), whereas initial pH was not  
422 significant (p-value of 0.3531). Unlike in other SSF processes [46], the variation of the initial  
423 pH in the range studied was not crucial on the response, because the effect of this factor depends  
424 on the strain, raw material and type of pretreatment [39]. The coded coefficients of the  
425 significant linear effects showed the degree of importance of the factors on the response: yeast  
426 extract (0.6671) > enzyme (0.5290). The p-value of the quadratic effect of enzyme (Z<sub>1</sub>Z<sub>1</sub>) was  
427 0.0002, indicating that this variable had the greatest effect on butanol production. The rest of  
428 quadratic and two-way interaction effects were found to be not significant.

429 3.3.2 Conjugated effect of enzyme and yeast extract

430 The response surface plot of the final model equation is shown in Figure 2, where the  
431 combined effect of enzyme loading and yeast extract on butanol production at a constant initial  
432 pH of 6.4 (central point in the CCD) is presented. In this figure, the three-dimensional surface  
433 and the two-dimensional contours for the butanol concentration after 48 h are plotted. The  
434 surface plot shape shows the great effect of the enzyme loading in comparison with the effect  
435 of yeast extract concentration. In addition, the rounded shape of the contour plots reflects,  
436 besides ANOVA outcomes, that the interaction effect between both factors was weak. As it can  
437 be seen, there is a maximum on the butanol concentration within the range of the variables  
438 established in the experimental design. According to the second-order model, the optimal  
439 conditions of the significant factors needed to achieve a butanol concentration of 5.43 g L<sup>-1</sup>  
440 were an enzyme loading of 13.5 FPU g-dw<sup>-1</sup> and a yeast extract concentration of 4.7 g L<sup>-1</sup>. It  
441 should be noted that an enzyme loading higher than 16.3 FPU g-dw<sup>-1</sup> caused a sudden decrease  
442 in the butanol concentration. In the one-step process, apart from increasing the operational  
443 costs, a large enzyme load could be counterproductive by inhibiting bacterial growth, as other  
444 authors have already pointed out [46]. Yeast is essential for ABE fermentation from bacteria  
445 such as *C. acetobutylicum* DSM 792, unlike other sources of nitrogen such as NH<sub>4</sub>Cl and  
446 NaNO<sub>3</sub> [47]. Bacteria use nitrogen in the formation of nucleic acids, proteins and cell wall  
447 components [48], so the increase in yeast extract concentration is usually related to the  
448 improvement of growth, which would lead to an increase in sugar consumption and a greater  
449 butanol production [49]. However, Al-Shorgani et al. [50] observed that an excessive reduction  
450 of the C/N ratio inhibits butanol production despite favouring the growth of *C. acetobutylicum*  
451 YM1.

### 452 3.3.3 SSF model validation

453 The validation of the predicted optimal conditions from the CCD results was carried out  
454 in three replicates by using an enzyme loading of 13.5 FPU g-dw<sup>-1</sup>, a yeast extract concentration

455 of 4.7 g L<sup>-1</sup> and an initial pH of 6.4. The variation with time of the solvent concentration  
456 (acetone and butanol; ethanol was not detected), acid concentration (acetic and butyric acid),  
457 sugar concentration (glucose, xylose and arabinose) and pH are plotted in Figure 3a. Butanol  
458 concentration at 48 h ( $5.49 \pm 0.09$  g L<sup>-1</sup>) only differed by 1.09% from the value estimated from  
459 the model ( $5.43$  g L<sup>-1</sup>), suggesting the goodness of model fit to predict the butanol concentration.  
460 Butanol yield and productivity were obtained as  $0.306 \pm 0.004$  g g of consumed sugar<sup>-1</sup> and  
461  $0.114 \pm 0.002$  g L<sup>-1</sup> h<sup>-1</sup> respectively. No increase in butanol concentration was observed after  
462 48 h. Interestingly, 93% of the maximum value was already reached at 24 h, giving a  
463 productivity of  $0.212 \pm 0.004$  g L<sup>-1</sup> h<sup>-1</sup>. The production of solvents resulted in  $8.00 \pm 0.10$  g L<sup>-1</sup>  
464 of total ABE at 24 h, when the concentration of acetone reaches its highest value ( $2.92 \pm 0.04$   
465 g L<sup>-1</sup>), and  $8.40 \pm 0.15$  g L<sup>-1</sup> at 48 h. Ethanol was not detected in significant concentrations  
466 throughout the study, which is positive for further downstream. Glucose and xylose  
467 accumulation were observed during the first 12 h, then decreased rapidly, indicating that  
468 enzyme hydrolysis was not the rate-limiting step unlike bacterial metabolism. This reversed  
469 after 48 h, when a slight increase in sugars was observed in the fermentation broth. For  
470 comparison purposes, the run 7 of the 2<sup>4-1</sup> fractional factorial design of the SHF processes  
471 (highest butanol production for this configuration) was included in Figure 3b. One of the main  
472 observable differences is that in order to achieve the maximum butanol production ( $4.85$  g L<sup>-1</sup>  
473 <sup>1</sup>), 72 extra hours are required compared to the one-step process.

474 A comparison of the results of this study with those derived from the SHF and SSF  
475 processes reported in the literature is summarised in Table 6. Among the studies presented,  
476 different species of the genus *Clostridium* and different lignocellulosic substrates were used.  
477 When comparing butanol and ABE production, the achieved concentrations ( $5.5$  and  $8.4$  g L<sup>-1</sup>,  
478 respectively) were within the published values ( $4.0$ - $12.6$  g L<sup>-1</sup> for butanol and  $7.4$ - $19.8$  g L<sup>-1</sup> for  
479 ABE), although they were in the lower range due to the low sugar concentration derived from

480 the hydrolyzated RS. The yield values of butanol and ABE found in this study ( $0.31 \text{ g g}^{-1}$  and  
481  $0.47 \text{ g g}^{-1}$ ) were much higher than those achieved in the literature ( $0.16\text{-}0.20 \text{ g g}^{-1}$  and  $0.26\text{-}0.30$   
482  $\text{g g}^{-1}$ ), thus corroborating the notion that solvent production was limited not due to the capacity  
483 of the bacterial strain but rather to the limited release of sugars from the lignocellulosic material  
484 ( $22.98 \text{ g L}^{-1}$ ). This restriction is also indicated by the butanol ( $51 \text{ g kg RS}^{-1}$ ) and ABE-biomass  
485 ratio ( $77 \text{ g kg RS}^{-1}$ ); parameters reflecting the overall conversion from raw RS to solvents that  
486 need to be increased for a large-scale production. Besides the high yield, the productivity of  
487 butanol ( $0.11 \text{ g L}^{-1} \text{ h}^{-1}$ ) and ABE solvents ( $0.18 \text{ g L}^{-1} \text{ h}^{-1}$ ) was higher than that previously  
488 reported for the SSF process, where it takes between 72 to 144 h to reach the maximum  
489 concentration of butanol, unlike the 48 h required in our study. Compared with SHF from the  
490 literature, the values were even better, as reported productivities do not take into account the  
491 required time for the biomass saccharification (48–72 h more). This is of great interest, as high  
492 productivities are necessary to ensure an adequate butanol removal rate in in-situ product  
493 removal processes [52]. Further study is necessary in order to increase the release of sugars  
494 from the RS by enhancing the pretreatment method. The use of large concentrations of biomass  
495 can lead to problems such as inappropriate energy efficiency in microwave pretreatment [18],  
496 decrease of mass transfer [53] and decrease of substrate conversion due to enzymatic inhibition  
497 [54]. Therefore, investigations will be focus on improving the delignification and ash removal  
498 rather than to increase the biomass loading.

#### 499 **4 Conclusions**

500 The serious environmental problems arising from the consumption of fossil fuels are  
501 increasing interest in producing biobutanol from lignocellulosic waste as a promising  
502 alternative energy source. In this study we demonstrated the feasibility of using hydrolysed rice  
503 straw by microwave irradiation as a substrate. By an adequate selection of operational  
504 conditions, fermentation time was reduced to 48 h with nearly total consumption not only of

505 glucose, but also of xylose, resulting in high productivity which is a great advantage for scaling-  
506 up. Besides, the SSF process was shown to be a favourable configuration with the potential  
507 capability to reduce substantially the production cost when compared with a conventional SHF  
508 process. From these promising results, further research on pretreatment conditions in order to  
509 improve the release of sugar concentrations from saccharification are of great interest to  
510 increase the butanol-biomass ratio prior to scale-up.

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**Table 1.** 5-Level CCD of 3 variables for the SSF process.  $\alpha = 1.68$ .

Independent variables		Coded and real values				
		Level - $\alpha$	Level -1	Central point (0)	Level +1	Level + $\alpha$
Z <sub>1</sub>	Enzyme loading (FPU g-dw <sup>-1</sup> )	5.4	8.2	12.2	16.3	19.1
Z <sub>2</sub>	Initial pH	5.6	5.9	6.4	6.9	7.2
Z <sub>3</sub>	Yeast extract (g L <sup>-1</sup> )	0.5	1.5	3.0	4.5	5.5

**Table 2.** 2<sup>4-1</sup> fractional factorial design and experimental results for the SHF and for the SSF processes.

SHF Process					
Run	Real values				Response Butanol 48 h (g L <sup>-1</sup> )
	Yeast extract (g L <sup>-1</sup> )	FeSO <sub>4</sub> ·7H <sub>2</sub> O (g L <sup>-1</sup> )	Initial pH	Saccharification buffer	
1	2	0.01	6.4	50 mM acetate	4.68
2	2	0.02	6.4	50 mM citrate	3.13
3	2	0.02	7.4	50 mM acetate	4.78
4	2	0.01	7.4	50 mM citrate	2.72
5	4	0.02	6.4	50 mM acetate	4.84
6	4	0.01	6.4	50 mM citrate	3.16
7	4	0.01	7.4	50 mM acetate	4.85
8	4	0.02	7.4	50 mM citrate	3.05
SSF Process					
Run	Real values				Response Butanol 48 h (g L <sup>-1</sup> )
	Yeast extract (g L <sup>-1</sup> )	FeSO <sub>4</sub> ·7H <sub>2</sub> O (g L <sup>-1</sup> )	Initial pH	Enzyme loading (FPU g-dw <sup>-1</sup> )	
1	2	0.01	5.2	4.1	1.55
2	2	0.02	5.2	12.4	1.53
3	2	0.02	6.2	4.1	2.80
4	2	0.01	6.2	12.4	4.98
5	4	0.02	5.2	4.1	1.00
6	4	0.01	5.2	12.4	0.58
7	4	0.01	6.2	4.1	1.28
8	4	0.02	6.2	12.4	5.24

**Table 3.** Comparison of SHF and SSF processes after 48 h of fermentation.

Method	Released Sugars (g L <sup>-1</sup> ) <sup>a</sup>		Butanol (ABE) Production	Butanol(ABE) Yield	Butanol (ABE)-biomass Ratio	Butanol (ABE) Productivity
	Glucose	Xylose	(g L <sup>-1</sup> )	(g g <sup>-1</sup> )	(g kg RS <sup>-1</sup> )	(g L <sup>-1</sup> h <sup>-1</sup> )
SHF	17.68	6.10	4.85 (7.95)	0.245 (0.402)	44.6 (73.1)	0.040 (0.066)
SSF	18.92	6.91	5.24 (8.24)	0.217 (0.341)	48.2 (75.8)	0.109 (0.172)

<sup>a</sup> Sugars obtained after 72h of hydrolysis time. In the case of SSF, sugars released from two abiotic controls.

**Table 4.** CCD experimental matrix along with the observed and predicted values of the response for the SSF process.

Run	Real values			Butanol (g L <sup>-1</sup> )	
	Z <sub>1</sub>	Z <sub>2</sub>	Z <sub>3</sub>	Observed	Predicted
1	8.2	5.9	1.5	2.62	2.22
2	16.3	5.9	1.5	2.52	2.96
3	8.2	6.9	1.5	2.79	2.70
4	16.3	6.9	1.5	3.68	3.99
5	8.2	5.9	4.5	4.21	4.00
6	16.3	5.9	4.5	4.62	4.82
7	8.2	6.9	4.5	3.83	3.50
8	16.3	6.9	4.5	4.38	4.88
9	5.4	6.4	3.0	1.06	1.72
10	19.1	6.4	3.0	4.31	3.50
11	12.2	5.6	3.0	4.14	4.17
12	12.2	7.2	3.0	4.80	4.62
13	12.2	6.4	0.5	3.11	3.01
14	12.2	6.4	5.5	5.31	5.25
15	12.2	6.4	3.0	n.a. <sup>a</sup>	4.96
16	12.2	6.4	3.0	4.58	4.96
17	12.2	6.4	3.0	5.19	4.96
18	12.2	6.4	3.0	5.10	4.96
19	12.2	6.4	3.0	4.81	4.96
20	12.2	6.4	3.0	5.10	4.96

<sup>a</sup> n.a.: non available

**Table 5.** ANOVA of the second-order model for butanol production by SSF process.

Source	Degrees of freedom	Sum of squares	Mean square	<i>F</i> value	<i>p</i> -value Prob > F	Coefficient <sup>a</sup>
Model	9	20.6456	2.2940	9.04	0.0015	
Linear	3	10.1421	3.3807	13.33	0.0012	
Z <sub>1</sub> : Enzyme loading	1	3.8221	3.8221	15.07	0.0037	0.5290
Z <sub>2</sub> : Initial pH	1	0.2432	0.2432	0.96	0.3531	0.1334
Z <sub>3</sub> : Yeast extract	1	6.0768	6.0768	23.95	0.0009	0.6671
Square	3	9.8683	3.2894	12.97	0.0013	
Z <sub>1</sub> Z <sub>1</sub>	1	9.4120	9.4120	37.10	0.0002	-0.8304
Z <sub>2</sub> Z <sub>2</sub>	1	0.5516	0.5516	2.17	0.1744	-0.2010
Z <sub>3</sub> Z <sub>3</sub>	1	1.1750	1.1750	4.63	0.0598	-0.2934
2-way interactions	3	0.6353	0.2118	0.83	0.5079	
Z <sub>1</sub> Z <sub>2</sub>	1	0.1591	0.1591	0.63	0.4488	0.1410
Z <sub>1</sub> Z <sub>3</sub>	1	0.0035	0.0035	0.01	0.9086	0.0210
Z <sub>2</sub> Z <sub>3</sub>	1	0.4726	0.4726	1.86	0.2054	-0.2431
Error	9	2.2832	0.2537			
Lack-of-fit	5	2.0244	0.4049	6.26	0.0500	
Pure error	4	0.2588	0.0647			
Total	18	22.9288				
Standard Deviation, SD					0.5037	
R <sup>2</sup>					0.9004	
Adj. R <sup>2</sup>					0.8008	

<sup>a</sup> For coded variables.



**Table 6.** Comparison of ABE fermentation through SHF and SSF processes from different feedstocks.

Substrate	Pretreatment	Fermentation method	Pretreated biomass loading	Enzyme loading	Microorganism	Butanol (ABE) production (g L <sup>-1</sup> )	Butanol (ABE) yield (g g <sup>-1</sup> )	Butanol (ABE)-biomass ratio (g kg RS <sup>-1</sup> )	Butanol (ABE) Productivity (g L <sup>-1</sup> h <sup>-1</sup> )	Reference
Brewer's spent grain	Dilute acid hydrolysis	SHF	10% (w/w)	Celluclast 1.5L (15 FPU g-dw <sup>-1</sup> ), Novozyme 188 (15 IU g-dw <sup>-1</sup> )	<i>C. beijerinckii</i> DSM 6422	6.1 (8.2)	0.20 (0.26)	28 (38)	0.06 (0.08)**	[51]
Rice straw	Ethanol organosolv	SHF	8% (w/w)	Celluclast 1.5L (25 FPU g-dw <sup>-1</sup> ), Novozyme 188 (40 IU g-dw <sup>-1</sup> )	<i>C. acetobutylicum</i> NRRL B-591	7.1 (10.5)	-	70 (103)	0.10 (0.15)**	[34]
Paper sludge	None	SSF	5% (w/v)	Cellic CTec2 (15 FPU g glucan <sup>-1</sup> )	<i>C. acetobutylicum</i> ATCC 824	8.5 (14.5)	0.18 (0.30)	92 (157)	0.07 (0.12)	[45]
Oil palm empty fruit bunch	Alkaline	SSF	5% (w/v)	Acremonium cellulase (15 FPU g-dw <sup>-1</sup> )	<i>C. acetobutylicum</i> ATCC 824	4.0 (7.4)	0.16 (0.30)	80 (148)*	0.03 (0.06)	[46]
Wheat straw	Ammonium sulfite	SSF	9% (w/v)	Cellulase (5 FPU g-dw <sup>-1</sup> ), Xylanase (10 IU g-dw <sup>-1</sup> )	<i>C. acetobutylicum</i> ATCC 824	12.6 (19.8)	-	110 (173)	0.09 (0.14)	[12]
Rice straw	Microwave assisted hydrothermolysis	SSF	9% (w/v)	Cellic CTec2 (12 FPU g glucan <sup>-1</sup> )	<i>C. beijerinckii</i> DSM 6422	5.5 (8.4)	0.31 (0.47)	51 (77)	0.11 (0.18)	This study

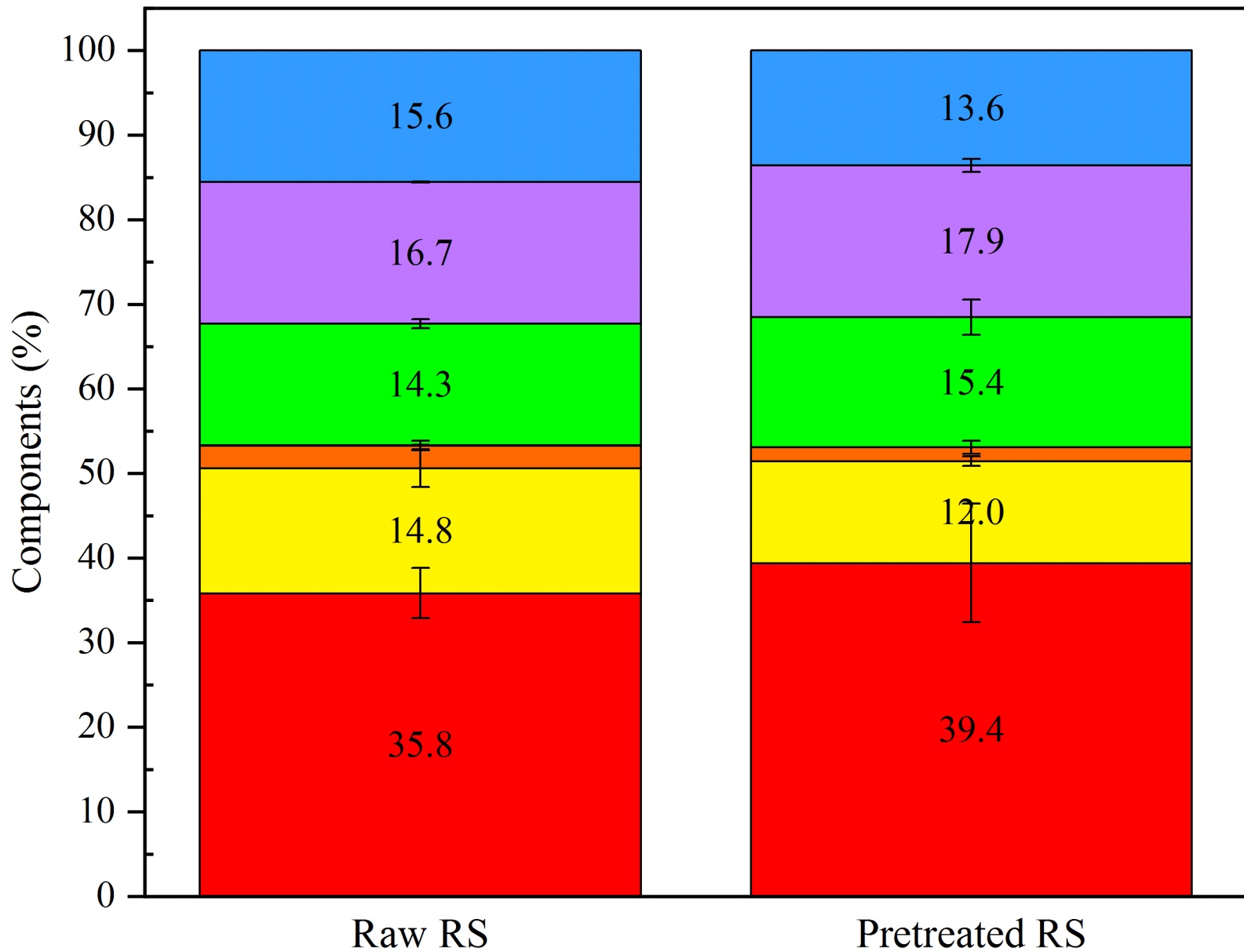
\*The butanol and ABE-biomass ratio was calculated considering that the solid recovery was 100%.

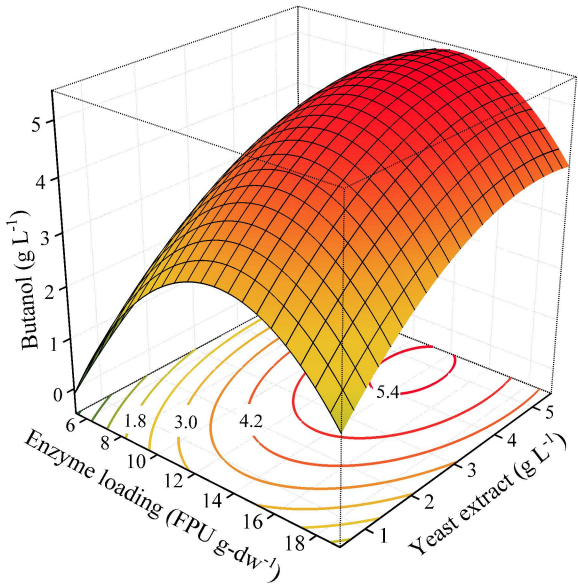
\*\*The butanol and ABE productivity was calculated without considering the enzymatic hydrolysis time.

**Figure 1.** Chemical composition of raw and pretreated rice straw.

**Figure 2.** The response surface and the corresponding contour plot for butanol production ( $\text{g L}^{-1}$ ) at 48 h in the SSF process: combined effect of enzyme loading ( $\text{FPU g-dw}^{-1}$ ) and yeast extract concentration ( $\text{g L}^{-1}$ ). Initial pH = 6.4.

**Figure 3.** Comparison of SSF and SHF processes. (a) SSF: CCD model validation at the predicted optimum conditions. Standard bar errors from three replicates; (b) SHF: Best results achieved, single run 7 of the  $2^{4-1}$  fractional factorial design.





● pH    Products: ○ Acetone    ▲ Butanol    ◊ ABE    ☆ Acetic acid    ▽ Butyric acid  
 Sugars:    ▷ Arabinose    ■ Glucose    ◆ Xylose

